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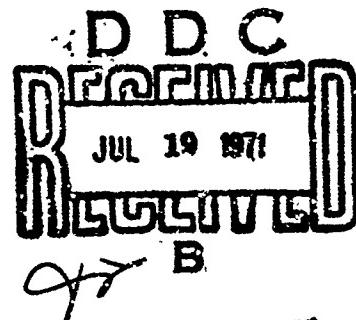
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# THEORETICAL GUN PROPELLANT THERMOCHEMICAL EVALUATION

GUNS AND ROCKETS BRANCH  
ADVANCED DEVELOPMENT DIVISION

TECHNICAL REPORT AFATL-TR-71-11

JANUARY 1971



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# **Theoretical Gun Propellant Thermochemical Evaluation**

**Otto K. Heiney**

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Base, Florida 32542.

FOREWORD

This report has been generated under the advanced gun propellant evaluation analysis portion of Project 62602F 2560 and is presented as a state of the art advancement that can be applied to gun propellant research efforts. The study was conducted during the period February 1970 to January 1971.

This technical report has been reviewed and is approved.



CHARLES PETRIDES  
Chief, Advanced Development Division

## ABSTRACT

A computer program is presented for computing the chemical equilibrium reaction products associated with gun propellant combustion. This program will provide a good first approximation of flame temperature, specific heat ratio, impetus, and mean molecular weight of the combustion products. The program as developed at the Air Force Armament Laboratory was based on a code used by the National Aeronautics and Space Administration Lewis Research Center. The minor changes to the program are discussed, some results from advanced solid propellant formulations calculations are presented, and a form of users manual for thermochemical programs and for the program to generate specific heat polynomials from JANAF tabular data is presented.

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## LIST OF ABBREVIATIONS AND SYMBOLS

C <sub>p</sub>	Specific heat at constant pressure
C <sub>v</sub>	Specific heat at constant volume
E	Internal energy
F <sub>p</sub>	Propellant impetus
G	Gibbs free energy
H	Enthalpy
K	Gas conductivity
M	Molecular weight
P	Pressure
R	Gas constant
S	Entropy
T	Temperature
T <sub>FP</sub>	Flame temperature at constant pressure
T <sub>FV</sub>	Flame temperature at constant volume
V	Volume
x <sub>i</sub>	Mole fraction
γ	Specific heat ratio
σ	Leonard-Jones force constant
Ω	Leonard-Jones force constant
μ	Gas viscosity

## SECTION I

### INTRODUCTION

The field of gun propellant development, which had been relatively static for many years, has recently begun to attract increased attention. The availability of an accurate theoretical thermochemical propellant performance computer program is of central importance to informed research and development efforts in this field. As a formulation screening tool, a few dollars of machine time can save hundreds of dollars of laboratory small-batch-mix effort by eliminating unpromising candidate formulations and providing a good first approximation to the primary important propellant parameters. These would include flame temperature, specific heat ratio, impetus, and mean molecular weight of the combustion products. To most expediently obtain a computer program for computing the chemical equilibrium reaction products, the Air Force Armament Laboratory modified an existing free-energy minimization rocket propellant performance program. The program selected was the one used by the National Aeronautics and Space Administration Lewis Research Center. This code<sup>(1)</sup> has a background of almost ten years of successful application. In addition, it was readily available and the JANAF specific heat data could be easily applied to the thermodynamic data tape. The program, as modified for gun propellant applications, was checked against established experimental data and other analytic chemical equilibrium computing techniques, with excellent agreement. Additionally, an algorithm was added which computes combustion gas viscosity and thermal conductivity by a Leonard-Jones potential technique.

The following sections of this report discuss the minor changes made to the Lewis approach, give some results from advanced solid propellant formulation calculations, and provide a form of users manual for the thermochemical programs and for the program to generate specific heat polynomials from JANAF tabular data<sup>(2)</sup>. Appendix I presents the Lewis program listing and Appendix II presents the polynomial fit program used at the Armament Laboratory.

## SECTION II

### FREE ENTHALPY EQUATIONS

This report will not discuss the mathematical techniques of chemical equilibrium computations. This task has effectively been accomplished in a recently issued monograph<sup>(3)</sup> which discusses in detail not only the Lewis technique but also several other commonly used approaches. This report will demonstrate only that, at chemical equilibrium, the Gibbs free energy, G, (or free enthalpy) will be a minimum.

From the First Law of Thermodynamics, in an irreversible process:

$$dE + pdv - Tds < 0 \quad (1)$$

or at equilibrium

$$dE + pdv - Tds = 0 \quad (2)$$

For a constant pressure and temperature, equation (2) becomes

$$d(E + pv - Ts) = 0 \quad (3)$$

$$G_T = H_T - T_1 S_1 \quad (4)$$

Equation (4) establishes the relation that the Gibbs free energy will be a minimum at equilibrium, and when coupled with the atomic species mass conservation equations, it provides a sufficient set for solution of the combustion species concentration and flame temperature (if the combustion pressure is specified). Then, to set up a minimization algorithm only requires a value for the heat of formation of the reactant compounds and tabular or polynomial data for the specified heat,  $C_p$ , enthalpy,  $H_T$ , and entropy,  $S_T$ , of the possible combustion products. These thermodynamic data can be obtained from reference 2 for most combustion products of interest: as

$$H_T - H_{298} = \int_{298}^T C_p dT \quad (5)$$

$$\text{and } S_T - S_{298} = \int_{298}^T \frac{C_p}{T} dT \quad (6)$$

Selecting a polynomial form for  $C_p$ , the terms  $H_T$  and  $S_T$  can be conveniently fitted to similar polynomials by performing the indicated integrations

$$\frac{C_p}{R} = a_1 + a_2T + a_3T^2 + a_4T^3 + a_5T^4 \quad (7)$$

$$\frac{H_T}{RT} = a_1 + 1/2 a_2T + 1/3 a_3T^2 + 1/4 a_4T^3 + 1/5 a_5T^4 + a_6/T \quad (8)$$

$$\frac{S_T}{R} = a_1 \ln T + a_2T + 1/2 a_3T^2 + 1/3 a_4T^3 + 1/4 a_5T^4 + a_7 \quad (9)$$

For a more precise fit, the Lewis program utilizes two sets of coefficients for each species, one in the temperature range 0° to 1000°K and the other from 1000° to 6000°K. Limits of species existence can be placed on the propellant data to restrict the range of polynomial applicability.

The primary change made to the Lewis algorithm was to additionally develop an approximate isochoric temperature from the isobaric temperature provided by the program. This requires the assumption that approximately the same species would form either in an isochoric or isobaric process, providing a similar total heat release. If these assumptions are warranted, then:

$$Q_R = C_p T_{Fp} \quad (10)$$

$$Q_R = C_V T_{FV} \quad (11)$$

$$T_{FV} = C_p / C_V T_{Fp} = \gamma T_{Fp} \quad (12)$$

Once the isochoric flame temperature and mean molecular weight of the combustion products are known, the impetus is simply

$$F_p = \frac{R}{M} T_{FV} \quad (13)$$

where  $R = 2780 \text{ ft-lbs/lb-mole}^{-\circ}\text{K}$

The program also computes the constitutive products mole fractions as a function of the pressure ratio (or, for a gun system, of the velocity) if quasi-isentropic conditions are assumed.

Equation (13) indicates the importance of developing advanced propellants with lower molecular weight combustion products, if the impetus

of a propellant is to be increased without a corresponding flame temperature increase. High propellant flame temperatures are, of course, the prime limiting factor in developing an acceptable barrel life for automatic aircraft cannon having a high performance and a high rate of fire. Current single-base solid gun propellants display molecular weights in the order of 25. Table I illustrates the distinctive flame temperature advantage of lower molecular weights in obtaining cooler combustion conditions without sacrificing energy output.

TABLE I. FLAME TEMPERATURES AS A FUNCTION OF MOLECULAR WEIGHT AND IMPETUS

Molecular Weight, Atomic Mass Units	Flame Temperature, °K, at Impetus, Ft-lb/lb			
	325,000	350,000	375,000	400,000
25	2980	2150	3380	3500
22	2570	2770	2970	3170
20	2340	2620	2700	2880
19	2220	2390	2570	2740
18	2110	2270	2430	2590
17	1990	2140	2290	2450

The very favorable performance data indicated by the lower right-hand entries in Table I are responsible for the continued advanced solid gun propellant development efforts. The test cases described in the following sections have resulted from calculations of two of the formulations now under contract investigation and from a comparison of results of two theoretical computations with experimental measurements of inservice propellants. All computations are performed at a standard reference pressure of 5,000 psia.

The first requirement for free energy computations is a reliable list of heats of formations for the constituents to be considered. Table II provides this data for the ingredients in the formulations discussed in this report. Additional tables are available in references 4 and 5.

TABLE II. HEATS OF FORMATION

CONSTITUENT	EMPIRICAL FORMULA	HEATS OF FORMATION KILOCALORIES PER MOLE
Ammonium Nitrate	H <sub>4</sub> O <sub>3</sub> N <sub>2</sub>	-88.1
CTPB	C <sub>7</sub> H <sub>11</sub> O <sub>2</sub> N <sub>0.02</sub>	-5.0
Dibutylphthalate	C <sub>18</sub> H <sub>14</sub> O <sub>4</sub>	-200.0
Diphenylamine	C <sub>12</sub> H <sub>11</sub> N <sub>1</sub>	+27.6
DMDTH	N <sub>4</sub>	-94.0
Ethyl Acrylate	C <sub>6</sub> H <sub>8</sub> O <sub>2</sub>	-87.3
Ethyl Alcohol	C <sub>2</sub> H <sub>6</sub> O <sub>1</sub>	-66.3
Ethyl Centralite	C <sub>17</sub> H <sub>20</sub> O <sub>1</sub> N <sub>2</sub>	-34.2
Ethylene Dihydrazine	C <sub>2</sub> H <sub>10</sub> N <sub>4</sub>	+31.2
Glycol Dinitrate	C <sub>2</sub> H <sub>4</sub> O <sub>6</sub> N <sub>2</sub>	-58.7
Guanidine Nitrate	C <sub>1</sub> H <sub>6</sub> O <sub>3</sub> N <sub>4</sub>	-79.3
HMX	C <sub>4</sub> H <sub>8</sub> O <sub>8</sub> N <sub>8</sub> S <sub>12</sub>	+17.9
Nitrocellulose (12.6 percent N)	C <sub>24</sub> H <sub>30</sub> O <sub>2</sub> N <sub>9.8</sub>	-655.5
Nitrocellulose (12.7 percent N)	C <sub>24</sub> H <sub>30</sub> O <sub>40</sub> N <sub>10.0</sub>	-659.3
Nitrocellulose (13.15 percent N)	C <sub>24</sub> H <sub>29</sub> O <sub>5</sub> N <sub>10.6</sub>	-643.1
Nitrocellulose (13.75 percent N)	C <sub>24</sub> H <sub>29</sub> O <sub>3</sub> N <sub>10.7</sub>	-639.9
Nitroglycerine	C <sub>3</sub> H <sub>5</sub> O <sub>9</sub> N <sub>3</sub>	-85.3
Nitroguanidine	C <sub>1</sub> H <sub>4</sub> O <sub>2</sub> N <sub>4</sub>	-12.6
Polymethyl Vinyl Tetrazole	C <sub>4</sub> H <sub>6</sub> N <sub>4</sub>	+52.4
RDX	C <sub>3</sub> H <sub>6</sub> O <sub>6</sub> N <sub>6</sub>	+14.9
Potassium Sulfate	K <sub>2</sub> S <sub>1</sub> C <sub>4</sub>	-338.5
Triacetin	C <sub>9</sub> H <sub>14</sub> O <sub>6</sub>	-307.0
Triazoethanol	C <sub>2</sub> H <sub>5</sub> O <sub>1</sub> N <sub>3</sub>	+22.5
Triaminoguanidine Nitrate	C <sub>1</sub> H <sub>9</sub> O <sub>5</sub> N <sub>7</sub>	-11.5
Water	H <sub>2</sub> O <sub>1</sub>	-68.4

### SECTION III

#### COMPUTATION OF VISCOSITY AND CONDUCTIVITY

For gun propellant applications, it is often quite important to determine a theoretical value for the combustion gas conductivity and viscosity. These are particularly necessary if the convective gun barrel heating characteristics of the propellants are to be evaluated. To accomplish this task, the Leonard-Jones potential technique<sup>(6)</sup> was applied.

The viscosity for a single constitutive species is given by:

$$\mu_1 = 2.6693 \times 10^{-5} \sqrt{MT} / \sigma^2 \Omega \quad (14)$$

where T is the temperature, M is the molecular weight, and  $\sigma$  and  $\Omega$  are the Leonard-Jones force constants. The viscosity of the mixture is defined by

$$\mu_{MIX} = \sum_{i=1}^n \left( x_i \mu_i \right) / \left( \sum_{j=1}^n x_j \phi_{ij} \right) \quad (15)$$

with n being the number of species considered and  $x_i$  being the mole fraction of the species. The value,  $\phi_{ij}$  is defined as

$$\phi_{ij} = \frac{1}{\sqrt{8}} \left( 1 + \frac{M_i}{M_j} \right)^{-1/2} \left[ 1 + \left( \frac{\mu_i}{\mu_j} \right)^{1/2} \left( \frac{M_j}{M_i} \right)^{1/4} \right]^2 \quad (16)$$

The thermal conductivity of a species is given as:

$$K_i = 1.9891 \times 10^{-4} \frac{\sqrt{TM}}{\sigma^2 \Omega} \quad (17)$$

The mixture value is given as

$$K_{MIX} = \sum_{i=1}^n \left( x_i k_i \right) / \left( \sum_{j=1}^n x_j \phi_{ij} \right) \quad (18)$$

This approach is strictly valid for only dilute mixtures of non-polar molecules. Five species are considered, (one of which, H<sub>2</sub>O, is polar), and all have a dense gas system. Thus, the results contain only order of magnitude validity, but are none the less of value, considering the state of the art in mathematical modeling of the transient heat convection process in gun bores. Table III gives the species considered which are typically 98 to 99 percent of the combustion gas constituents.

TABLE III. LEONARD-JONES POTENTIAL PARAMETERS (FORCE CONSTANTS)

Species	Molecular Weight, Atomic Mass Units	Viscosity, Grams/cm-sec	Conductivity, Cal/cm-sec-K
H <sub>2</sub>	2.016	2.915	38.0
N <sub>2</sub>	28.02	3.749	79.8
CO	28.01	3.706	88.
CO <sub>2</sub>	44.01	3.897	213.
H <sub>2</sub> O	18.0	2.824	230.9

Table IV consists of the  $\Omega$ - $\frac{KT}{\epsilon}$  relations needed for the solution of Equations (14) and (17). The first column contains values for the relatively non-polar species such as H<sub>2</sub>, N<sub>2</sub>, CO, and CO<sub>2</sub>, while the second column has a corrected value for the highly polar H<sub>2</sub>O.

TABLE IV. REDUCED CROSS SECTION

KT / ε	NON-POLAR	POLAR		KT / ε	NON-POLAR	POLAR
1.0	1.5938	2.6199		7	0.8725	0.8946
1.2	1.4568	2.4257		8	0.8536	0.8422
1.4	1.3557	2.2713		9	0.8378	0.8043
1.6	1.2800	2.1413		10	0.8242	0.7760
1.8	1.2216	2.0263		11	0.8123	0.7544
2.0	1.1751	1.9217		12	0.8017	0.7376
2.2	1.1377	1.8258		13	0.7922	0.7243
2.4	1.1066	1.7373		14	0.7836	0.7134
2.6	1.0803	1.6559		15	0.7756	0.7045
2.8	1.0579	1.5812		16	0.7883	0.6971
3.0	1.0385	1.5126		32	0.6939	0.6462
3.2	1.0214	1.4499		64	0.6262	0.6033
3.4	1.0063	1.3926		128	0.5634	0.5528
3.6	0.9928	1.3401		256	0.5056	0.5006
3.8	0.9807	1.2922		512	0.4528	0.4505
4.0	0.9696	1.2485				
5.0	0.9265	1.0797				
6.0	0.8960	0.9694				

## SECTION IV

### INPUT FOR GUN PROPELLANT PROGRAM

The input data for the gun propellant program (Appendix I) can be divided into four general groups having code names as follows:

- 1) Thermodynamic data for the reaction products (THERMØ data).
- 2) Data pertaining to the reactants or propellants (REACTANTS data).
- 3) Special options related to chemical species present in the combusted gas (ØMIT/INSERT data).
- 4) Namelist data including the type of problem, pressure ratio and area ratio schedules, various options, etc. (NAMELISTS data).

The required order of the data cards is:

- 1) One card with the code word THERMØ punched in columns 1 to 6.
- 2) THERMØ data.
- 3) REACTANTS card. Number of reactants right adjusted in columns 1 to 3 and number of cases right adjusted in columns 4 to 6.
- 4) ØMIT and/or INSERT data.
- 5) One card containing up to 80 columns of alphanumeric identification data.
- 6) NAMELISTS data.

For any particular problem there may be multiple REACTANTS cards. Each set of REACTANTS cards may be followed by multiple NAMELISTS input cards. Each type of input data is discussed in detail in the following sections.

#### 1. THERMØ DATA

The thermodynamic data for the reaction products may be read either from cards or from magnetic tape. When tape input is used, both the THERMØ code card and all THERMØ data cards must be omitted. It is anticipated that most users will prefer the magnetic tape since this reduces the number of cards which must be handled. The card format for the THERMØ data is described in Section V. Use of the tape input requires no action on the part of the user, once the required data is established on the tape.

#### 2. REACTANTS DATA

REACTANTS data is required for all problems. Following the code card there should follow one card for each reactant species being considered, with a maximum of 15 allowed. Each reactant card, after the code card, contains the following information:

- a. The chemical formula for the species.
- b. Either the number of moles of the reactant or the relative weight. The relative weight is the weight of each fuel or oxidizer expressed as a fraction of the total fuel or oxidizer.
- c. The enthalpy of the species expressed in calories per mole. (This is not required for an assigned temperature problem. See Section IV.4 for description of assigned temperature problem.)
- d. The state of the reactant (gas, liquid, or solid).
- e. The temperature associated with the enthalpy.
- f. Designation of each reactant species as either a fuel or an oxidizer. (The program then combines all fuels into an effective fuel and all oxidizers into an effective oxidizer.)
- g. The reactant species density. (This information is optional and may be omitted. If densities are input for all reactants, the program calculates a density for the overall system.)
- h. Multiple cases with identical reactants are identified by the reactants code card and the preceding data need not be repeated.

The reactant information is arranged on a card. Standard chemical alphabetic symbols are required for the chemical elements (i.e., H for hydrogen, HE for helium, LI for lithium, BE for beryllium, etc.). Each reactant may be composed of no more than five distinct chemical elements. Each chemical element is allowed two columns (columns 1 and 2, 10 and 11, 19 and 20, 28 and 29, and 37 and 38) for its symbol. For those elements whose symbol consists of a single letter, the symbol must be placed in the left-most (left adjusted) of the two columns. The formula number (the number of atoms of each element in a reactant) is to appear in the columns immediately following the chemical symbol (i.e., columns 3 to 9, 12 to 18, 21 to 27, 30 to 36, and 39 to 45). The formula number may appear anywhere within the seven column field, and a decimal point must be used for each number. Note that the exponent numeric form, or E format, may not be used here. Also note that for a given reactant an individual element may appear only once (empirical formula). Thus, a compound such as furfuryl alcohol, whose formula might be written as C<sub>4</sub>H<sub>30</sub>·CH<sub>2</sub>OH to represent its structure, must be treated as though it were C<sub>5</sub>H<sub>6</sub>O<sub>2</sub> or O<sub>2</sub>H<sub>6</sub>C<sub>5</sub>, etc. The order of the elements is immaterial for this program.

The relative weight of each reactant should be placed in columns 46 to 52. The number may appear anywhere in these columns, a decimal point must be used, and the exponent numeric form may not be used. If the number of moles of each species is input in these columns the same restrictions apply, but an additional bit of information, an M in column 53, must

appear on the card. Column 53 is left blank for relative weights. Note that the relative weight and molar designations may not be mixed for any single problem.

The reactant enthalpy is placed in columns 54 to 62, and the units must be calories per mole. The number may appear anywhere in these columns, a decimal point must be used, and the exponent numeric form may not be used. A sign is required only if the enthalpy is negative. Obviously, this enthalpy must be consistent with the enthalpy base used for the THERM $\phi$  data. For the JANAF data, the enthalpy base is as follows: For each element, the phase, condensed or liquid, which is most stable at one atmosphere pressure is designated as a reference, or base, state. The heat of formation of this state at 298.15°K is arbitrarily specified as zero. Then all thermodynamic properties for other phases of the element, as well as for any compound containing the element, are referenced to the base state.

The initial state for each reactant is indicated by an S for solid, an L for liquid, or a G for gas in column 63. The initial reactant temperature, in degrees Kelvin, goes in columns 64 to 71. Both the initial state and temperature are used only to label the output printout and if they are omitted or input incorrectly, the calculations are not affected.

For all problem types (see Section IV.4) except a detonation problem, columns 73 to 70 are reserved for the reactant density in grams per cubic centimeter. The inputting of this data is optional, but if it is given, a decimal point must be used. For a detonation problem, columns 73 to 80 are used for the reactant specific heat at constant pressures. This data is required for each reactant for a detonation problem.

### 3. OMIT/INSERT DATA

The purpose of the OMIT/INSERT option is as follows. The program considers as possible products all species in the THERM $\phi$  data which are consistent with the chemical system which was input on the REACTANTS cards. Occasionally, it may be desired to eliminate one or more species from consideration as possible products. This may be accomplished by placing the species chemical formula on an OMIT card. Both gaseous and condensed species may be omitted.

Only the names of condensed species may appear on an INSERT card. The INSERT option has been included for two reasons. The less important of the two is that if it is known beforehand that one or more particular condensed species will be among the final equilibrium composition for the first assigned point (i.e., the combustion chamber for a rocket problem), then a small amount of computer time can be saved by using an INSERT card. The more important reason for the INSERT option is that, in rare instances, it is impossible to obtain convergence without the use of an

INSERT card. This occurs when, by considering gases only, the temperature becomes extremely low. When this happens, the program outputs the following message: "LOW TEMPERATURE IMPLIES CONDENSED SPECIES SHOULD HAVE BEEN INCLUDED ON AN INSERT CARD" and no solution will be obtained. The user should resubmit the problem with one or more appropriate condensed species listed on an INSERT card.

The use of OMIT and INSERT cards is completely optional; however when used, each card must contain either the code word OMIT in columns 1 to 4 or INSERT in columns 1 to 6 and the chemical formulas of from one to four product species. The names of the species must be left-adjusted and begin in columns 16, 31, 46, or 61. In addition, the species name must be punched on the card exactly as it appears in the THERM<sub>D</sub> data. This means that the order of the chemical elements within the species name, the formula numbers, and the state of the species must all be identical. For example, gaseous ammonia would commonly appear as NH<sub>3</sub>. Because of the alphabetizing scheme used for thermodynamic data, this species is written as H3N1(G).

#### 4. NAMELISTS DATA

The word NAMELIST is a FORTRAN IV statement and provides a convenient way of inputting data. One of the major advantages of the NAMELIST input method is that the data can be placed in any order and need not be placed within pre-specified card columns as is the case for the REACTANTS data. A secondary advantage is that the variable name appears with its numerical value on a card, thus making it easy to tell the purpose of each piece of data without having to refer to a program manual or to the program listing. Even though inputting data by means of NAMELIST is convenient, the following rules must be observed.

All data input by means of a NAMELIST statement must be associated with a NAMELIST name, and for this program there are only two: INPT2 and RKTINP. The first column of all NAMELIST data cards may not be used and must be blank. The second column of the first card only must contain a \$ character. The applicable NAMELIST name must be placed on the first card only. The name must begin in column 3, and must be followed by at least one blank column.

Each NAMELIST name is assigned a group of FORTRAN variables. (The variables belonging to INPT2 and RKTINP are listed in Tables V and VI, respectively.) These variables are assigned to a NAMELIST name within the program, and numeric data can only be input in conjunction with a NAMELIST name.

Although, in general, there are seven forms that input data may take, only three are of interest for this report. These are integer constants,

real number constants, and logical constants. These are defined as follows:

- a. An integer consists of one to eleven digits written without a decimal point.
- b. A real number constant may be written in two ways. The first form is from one to nine digits, including a decimal point, followed by an exponent. The exponent is written as the letter E followed by a sign and a one or two digit integer. For example 12345. could be written as 1.2345E04 or .12345+5, etc. The second form is one to nine digits, including a decimal point, but not followed by an exponent.
- c. A logical constant may be either true or false. There are two forms in which the constant may be written. These are either .TRUE. or T .FALSE. or F. The periods before and after the long forms are mandatory.

Logical constants may be associated only with logical variables. Integer constants may be associated with real variables and vice versa, and the proper conversion is made automatically by the computer. Note that when inputting data without a NAMELIST statement this conversion may cause difficulties and should only be used with great care.

On a NAMELIST card, each piece of data must be written in conjunction with its variable name (e.g., P = 100; or INDEX = 3, or PSIA = .TRUE., etc.). The equal sign is mandatory, and the data items must be separated by commas. If more than one card is required, the last item on each card, except for the last card, must be a constant followed by a comma. A variable name may not be the last item on the card. The end of a group of data is signaled by a \$ character. This may be on the same card as that containing the NAMELIST name if only one card is used or may be on any succeeding card, but it may not be the first character on a succeeding card. Note that it is not necessary to completely fill a card with data before beginning a subsequent card. In fact, the user may want to put each piece of data on separate cards. This facilitates subsequent data changes. One final note, it is not necessary to input data for every variable contained in a NAMELIST; however, each variable as been assigned a value within the program, and this value is used unless superseded by input data. The assigned values for all NAMELIST variables in this program are included in Tables V and VI.

To illustrate the preceding instructions, the following paragraphs discuss the specific NAMELIST data required by this program, what each data bit does, and then some specific examples.

The INPT2 NAMELIST data must be used for all problems. The variables in the INPT2 NAMELIST are listed and defined in Table V along with the type and assigned value of each variable. The type of problem (one of either TP, HP, RKT, or DETN), at least one pressure (P), and the relative amounts of fuel and oxidizer (i.e., one of either EQRAT, OF, FPCT, or FA) are required for each problem. The other variables are either completely optional or may be required only if a particular problem type is requested.

The variable JANF is a flag to indicate which thermodynamic data polynomial should be used. JANF=0 designates a polynomial of the form  $C_p = A_1 + A_2 T + A_3 T^2 + \frac{1}{4} A_4 T^3 + A_5 T^4$ . This is the form used by the Lewis Research Center and is also the form the Armament Laboratory uses after converting the JANAF data.

The Lewis program is quite flexible in the type of problems it will consider or the thermodynamic variables which may be fixed. For gun propellant problems, it is most advantageous to assign the enthalpy and pressure which, in system nomenclature, constitutes an RKT problem.

a. RKT Problem

If RKT = .TRUE. or T, then a rocket problem is solved. A rocket problem is one for which the combustion takes place at an assigned enthalpy (REACTANTS cards) and assigned pressure (single value in the P variable), followed by an isentropic expansion. The combustion temperature, the thermodynamic properties and rocket performance are calculated for the chamber, the throat, and assigned exit points. The exit points desired are specified in the RKTINP namelist. If a temperature is assigned (T variable), then combustion will be assumed to occur at that temperature and not at the assigned enthalpy. The RKT problem type combines the H,S and T,S problems of the earlier program version. Note that, when this option is selected, the second set of NAMELIST data, RKTINP, is then required. The combustion gas conductivity and viscosity are computed for this option only.

b. DETN Problem

If DETN = .TRUE. or T, then the program solves a Chapman-Jouget detonation problem. The thermodynamic properties and composition downstream of the detonation wave are calculated for an assigned pressure and temperature upstream of the wave. This detonation calculation is primarily oriented for gas phase detonations. It is of limited utility for computation of detonations in solids, as the specific heat polynomial of the reactants must be on the data tape, which will not, in general, be the case for a typical solid explosive constituent ingredient.

### c. P, PSIA, and MMHG Variables

The value P may be either the combustion pressure of a rocket engine (RKT problem) or a pressure at which composition and thermodynamic properties (TP or HP problem) are desired. Up to 26 values may be input, but only one is permitted for an RKT problem. The program assumes that the units of the pressures are in atmospheres unless either PSIA or MMHG are set true. If PSIA = .TRUE. or T then the pressure units are assumed to be in psia units. If MMHG = .TRUE. or T then the pressure units are assumed to be in millimeters of mercury. PSIA and MMHG may not both be set true in the same problem.

### d. T Variable

Values for the T variable should be input only if TP is set true or if an assigned chamber temperature is desired for RKT problem. The temperature units must be degrees Kelvin.

### e. EQRAT, $\emptyset F$ , FPCT, and FA Variables

The relative amounts of total fuel and total oxidizer may be expressed in one (and only one for each problem) of four ways. The mixture ratio ( $\emptyset F$ ) and percent fuel (FPCT) are self evident. The fuel-to-air weight ratio (FA) and equivalence ratio (EQRAT) are new to this version of the program and are not of use for gun propellant calculations.

### f. IDEBUG Variable

If IDEBUG = .TRUE. or T then a printout of the intermediate calculation details is obtained. This is intended primarily as a debugging aid in the event there are problems. The output is extensive and is explained on page 34 of Reference 1.

### g. I $\emptyset NS$ Variable

If I $\emptyset NS$  = .TRUE. or T then the program will consider ionized species. The earlier Lewis program version could not handle ionic species although provision was made in one of the subroutines for future consideration of ions. This capability is included in the newer program and thermodynamic data for ionized species are available as well as a sample problem which uses I $\emptyset NS$  = T.

### h. EQL, FR $\emptyset Z$ , PCP, SUBAR, and SUPAR Variables

The five RKTINP variables (EQL, FR $\emptyset Z$ , PCP, SUBAR, and SUPAR) in the RKTINP namelist are listed in Table VI. Of these, only PCP is required. The RKTINP namelist is required only if RKT is set true in the INPT2 namelist.

### (1) PCP Variable

The value PCP is the ratio of the chamber pressure to the exit pressure. This is one of the independent variables (along with the entropy) for the nozzle portion of a rocket problem, and as such, at least one value must be input. As many as 22 values may be input; however, unlike the older program, values for the chamber and throat should not be input. Pressure ratios for the subsonic portion of the nozzle may be used. Values must be ordered so that the magnitudes increase monotonically.

### (2) SUBAR and SUPAR Variables

Gun propellant performance at specific area ratios corresponding to a given gas velocity, either subsonic or supersonic, may be requested. Subsonic ratios are read as SUBAR and supersonic as SUPAR. When assigned area ratios are requested, the range of PCP values should be large enough to include the assigned area ratios. If the range is not large enough, extrapolation may be performed. SUBAR values should be ordered such that the values decrease and the SUPAR data should increase. Thirteen of each variable are permitted. Note that the use of this program feature is completely optional.

### (3) EQL and FRØZ Variables

The program will calculate performance for both equilibrium and frozen expansions unless instructed otherwise. If EQL = .FALSE. or F then the equilibrium expansion is omitted and only frozen performance is calculated. If FRØZ = .FALSE. or F then the frozen expansion is omitted and only equilibrium performance is calculated.

TABLE V. VARIABLES IN INPT2 NAMELIST

Variable Name	Variable Type	Value (Unless Set Differently)	Definitions
JANF	Integer	1.	Thermodynamic data polynomial indicator
P	Real	0.	Assigned pressures
T	Real	0.	Assigned temperatures
EQRAT	Real	0.	Equivalence ratio
ØF	Real	0.	Oxidant-to-fuel weight ratio
FPCT	Real	0.	Percent fuel by weight
FA	Real	0.	Fuel-to-air weight ratio
TP	Logical	False	Assigned temperature and pressure problem
HP	Logical	False	Assigned enthalpy and pressure problem
RKT	Logical	False	Rocket problem
DETN	Logical	False	Detonation problem
PSIA	Logical	False	Assigned pressure-to be in psia units
MMHG	Logical	False	Assigned pressures in millimeter of mercury units
IØNS	Logical	False	Consider ionic species
IDEBUG	Logical	False	Print intermediate output

TABLE VI. VARIABLES IN RKTINP NAMELIST

Variable Name	Variable Type	Value Unless Set Differently	Definition
EQL	Logical	True	Gun propellant performance assuming equilibrium composition to be calculated
FR $\emptyset$ Z	Logical	False	Gun propellant performance assuming frozen composition to be calculated
PCP	Real	0.	Ratio of chamber pressure to exit pressure
SUBAR	Real	0.	Subsonic area ratios
SUPAR	Real	0.	Supersonic area ratios

Table VII contains the input data for several propellant performance cases, and the output is listed on Tables VIII through XI. These cases are respectively M-10 (Case 100), M-9 (Case 101), an HMX-rubber propellant system (Case 102), and an RDX-triamino-guanidine nitrate formulation (Case 106). A comparison of these data with experimental or independent theoretical solutions gives the following results.

Case 100				
	Tv	Fp	Y	Mw
Lewis	3312	366,548	1.22	25.1
Experimental	3034	346,180	1.23	24.2
Case 101				
Lewis	3853	394,180	1.17	27.2
Experimental	3840	396,840	1.20	26.5
Case 102				
Lewis	2566	377,584	1.28	18.9
Other Theoretical	2545	373,000	(--)	18.9
Case 106				
Lewis	2637	390,870	1.29	18.8
Other Theoretical	2647	391,000	(--)	18.8

The input data (Table VII) are discussed in the program writeup except that no OMIT or INSERT cards are used.

## TABLE VII: INPUT DATA FOR SAMPLE GUN PROPELLANT PROBLEMS

3	1	C 24.0 H 29.5 O 41.3 N 10.6	1.0	-643100.	298.	F
C	12.0	H 11.0 N 11.0	.33	27600.	298.	O
C	2.0	H 14.0 O 6.0 N 4.0	.67	-66300.	298.	C
CASE	100	PROPELLANT IS M-10				
\$INPT2	JANF=0,P(1)=5000.,RKI=.TRUE.,FPCT=98.,PSIA=.TRUE.,\$					
\$RKTINP	PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=.FALSE.,\$					
4	1	C 24.0 H 29.5 O 41.3 N 10.6	1.0	-643100.	298.	E
C	3.0 C	H 5.0 O 9.0 N 3.0	.96	-85300.	298.	O
C	12.0	H 11.0 N 11.0 N 4.0	.02	27600.	298.	O
C	3.0	H 14.0 O 6.0	.02	-66300.	298.	O
CASE	101 PROPELLANT IS M-9					
\$INPT2	JANF=0,P(1)=5000.,RKI=.TRUE.,FPCT=58.,PSIA=.TRUE.,\$					
\$RKTINP	PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=.FALSE.,\$					
2	1	C 4.0 " H 8.0 O 8.0 N 8.0	1.0	17900.	298.	O
C	7.0	H 11.0 O 11.0 N 11.0	1.0	-5000.	298.	F
CASE	102 PROPELLANT IS HMX RUBBER					
\$INPT2	JANF=0,P(1)=5000.,RKI=.TRUE.,FPCT=15.,PSIA=.TRUE.,\$					
\$RKTINP	PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=.FALSE.,\$					
3	1	C 4.0 H 8.0 O 8.0 N 8.0	1.0	17900.	298.	O
C	7.0	H 11.0 O 11.0 N 11.0	.88	-5000.	298.	- F -
TITAN	PROPELLANT IS HMX-RUBBER WITH TITANIUM ADDED					
\$INPT2	JANF=0,P(1)=5000.,RKI=.TRUE.,FPCT=17.,PSIA=.TRUE.,\$					
\$RKTINP	PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=.FALSE.,\$					
4	1	C 2.0 H 5.0 O 1.0 N 3.0	.83	22500.	298.	F
C	4.0	H 6.0 N 4.0	.17	52400.	298.	F
C	3.0	H 6.0 O 6.0 N 6.0	.60	14900.	298.	O
C	1.0 H 9.0 O 3.0 N 7.0	.40	-11500.	298.	O	
CASE	106 PROPELLANT IS RDX-TAG NITRATE					
\$INPT2	JANF=0,P(1)=5000.,RKI=.TRUE.,FPCT=16.,PSIA=.TRUE.,\$					
\$RKTINP	PCP(1)=1.2,1.4,1.6,2.0,3.0,4.0,5.0,10.0,68.0,FROZ=.FALSE.,\$					

TABLE VIII. OUTPUT FOR CASE 100, M-10 PROPELLANT

THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING EQUILIBRIUM COMPOSITION DURING EXPANSION

CASE 100 PROPELLANT IS M-10		WT FRACTION ENTHALPY STATE TEMP DENSITY									
		(SEE NOTE) CAL/MOL DEG K G/CC									
FUEL	C 26.0000	H 29.5000	O 41.3000	N 13.6000							
OXIDANT	C 12.0000	H 11.0000	O 6.0000	N 4.0000							
OXIDANT C	2.00000	H 14.00000	O 6.00000	N 4.00000							
O/F =	.0204	PERCENT FUEL = 98.0000	EQUIVALENCE RATIO = 1.5547	DENSITY = 0.0000							
PC/P	CHAMBER	THROAT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT
P, ATM	1.0000	1.788	1.200	1.400	1.600	2.000	3.000	4.000	5.000	16.000	66.000
T, CP, DEG K	340.2	190.3	283.5	243.0	212.6	170.1	113.4	85.06	66.05	34.02	5.003
H, CAL/G	2713	2493	2625	2553	2491	2391	2217	2101	2015	1766	1227
S, CAL/G, (KJ)	-562.7	-681.0	-601.2	-632.7	-659.3	-702.4	-776.2	-825.3	-861.6	-965.8	-1189.2
M, MOL WT	25.125	25.137	25.130	25.133	25.135	25.138	25.141	25.143	25.144	25.146	
(OLV/OLP)T	-1.00052	-1.00022	-1.00040	-1.00032	-1.00010	-1.00019	-1.00010	-1.00005	-1.00007	-1.00003	-1.00030
TDC/VENT/DP	1.0096	1.0040	1.0074	1.0058	1.0047	1.0033	1.0017	1.0010	1.0007	1.0003	1.0037
CP, CAL/(G)(K)	.4447	.4313	.4398	.4362	.4334	.4294	.4239	.4209	.4191	.4152	.4239
GAMMA (S)	1.22206	1.22263	1.22226	1.22251	1.22272	1.2303	1.2316	1.2326	1.2352	1.2307	
SON VEL. M/SEC	1046.8	995.0	1030.5	1016.7	1004.8	985.1	949.7	906.2	849.6	786.6	
MACH NUMBER	8.000	7.000	5.51	7.53	8.95	1.096	1.408	1.603	1.745	2.168	3.240
VEL. FT/SEC	0.0	3266.4	1861.8	2511.7	2950.7	3547.5	4385.6	4863.7	5188.8	6819.9	7512.1
VISCO, SEC	0.00795	*.000738	*.000777	*.000762	*.000749	*.000727	*.000690	*.000655	*.000591	*.000466	
C, CAL/G-SEC-K	*.000300	*.000281	*.000294	*.000289	*.000285	*.000276	*.000266	*.000256	*.000251	*.000234	*.000281
T, DV, DEG K	3312	36654.8									
IMPELUS											
CSTAR, FT/SEC											
CP	4760	4760	4760	4760	4760	4760	4760	4760	4760	4760	4760
AE/AT	.886	.391	.328	.320	.745	.921	.921	.922	.920	.920	.920
IVAC,LB-SEC/18	1.000	1.266	1.065	1.011	1.008	1.036	1.036	1.036	1.036	1.036	1.036
I, LB-SEC/LB	184.2	213.9	190.5	185.1	184.8	192.3	199.0	209.2	219.6	251.3	233.5
101.5	57.9	78.1	91.7	110.3	136.3	151.2	161.3	187.1	233.5		

TABLE VIII. Concluded

MOLE FRACTIONS									
	CH <sub>4</sub>	C <sub>2</sub> H <sub>6</sub>	CO	CO <sub>2</sub>	H	HCN	HCO	H <sub>2</sub>	H <sub>2</sub> O
	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000
CH <sub>4</sub>	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000
CO	.40186	.39739	.40060	.39943	.39834	.39637	.39729	.36896	.36611
CO <sub>2</sub>	.13746	.14239	.13668	.14019	.14730	.14835	.15	.15092	.15376
H	.00104	.00046	.00082	.00066	.00054	.00039	.00020	.00012	.00031
HCN	.00001	.00001	.00001	.00001	.00011	.00001	.00001	.00002	.00000
HCO	.00016	.00008	.00013	.00011	.00009	.00007	.00004	.00002	.00000
H <sub>2</sub>	.10392	.10883	.10664	.10781	.10990	.11415	.11755	.12051	.12310
H <sub>2</sub> O	.23507	.23088	.23392	.23283	.23160	.22989	.22585	.22253	.21966
NH <sub>3</sub>	.00003	.00003	.00003	.00003	.00003	.00003	.00002	.00002	.00016
NO	.00005	.00001	.00004	.00002	.00002	.00001	.00000	.00002	.00002
N <sub>2</sub>	.11974	.11983	.11976	.11980	.11982	.11981	.11986	.11987	.11989
OH	.00061	.00019	.00043	.00032	.00024	.00015	.00006	.00003	.00001
ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS HERE LESS THAN .000005 FOR ALL ASSIGNED CONDITIONS									
C	C(S)	CH	CH <sub>2</sub>	CH <sub>3</sub>	CN	CH <sub>2</sub>	C <sub>2</sub> H	C <sub>2</sub> H <sub>2</sub>	C <sub>2</sub> H <sub>4</sub>
C <sub>2</sub> H <sub>4</sub>	C <sub>2</sub> N	C <sub>2</sub> N <sub>2</sub>	C <sub>2</sub> O	C <sub>3</sub>	H <sub>2</sub>	H <sub>2</sub> O(L)	H <sub>2</sub> O(S)	N	NH
NH <sub>2</sub>	N <sub>2</sub> C	N <sub>2</sub> C	N <sub>2</sub> H <sub>4</sub>	N <sub>2</sub> O	N <sub>2</sub> O <sub>4</sub>	O	O <sub>2</sub>		

NOTE.—WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS  
VISCOSITY AND CONDUCTIVITY VALUES BASED ON 99.0 PERCENT OF GAS MIXTURE

TABLE IX. OUTPUT FOR CASE 101, M-9 PROPELLANT

## THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING EQUILIBRIUM COMPOSITION DURING EXPANSION

PROPELLANT IS N-9									
CASE 101									
W/F FUSION ENTHALPY STATE TEMP DENSITY									
CASE	ITEM	NOTE	CAL/MOL	DEG K	G/CC				
CREMICAL FORMULA									
FUEL	C 24.00000	H 29.50000	0 41.30000	N 10.60000	-64310.000	290.00	-0.0008		
OXIDANT	C 3.00000	H 5.00000	O 9.00000	N 3.00000	-85300.000	290.00	-0.0008		
OXIDANT	C 12.00000	H 11.00000	N 1.00000	N 4.00000	.02000	27660.000	290.50	-0.0008	
OXIDANT	C 3.00000	H 14.00000	O 6.00000	O 6.00000	.02000	-66300.000	290.00	-0.0008	
PERCENT FUEL = 58.0000 EQUIVALENCE RATIO = 1.3101 DENSITY = 1.3101									
07F = .7741	PERCENT FUEL = 58.0000	EQUIVALENCE RATIO = 1.3101	DENSITY = 1.3101						
CHAMBER	THRUST	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT
PC/P	1.000	1.759	1.200	1.400	1.600	2.000	3.000	4.000	5.000
P, ATM	340.2	193.4	283.5	243.9	212.0	170.1	113.4	85.06	66.05
T, CP, DEG K	329.8	304.9	321.7	314.9	309.1	299.2	281.5	269.0	259.4
H, CAL/G	-685.1	-615.8	-522.8	-528.5	-564.3	-654.0	-729.4	-786.6	-829.3
S, CAL/(G) (K)	2.2389	2.2389	2.2389	2.2389	2.2389	2.2389	2.2389	2.2389	2.2389
M, MOL WT	27.185	27.319	27.271	27.300	27.342	27.398	27.426	27.441	27.466
COLV/DL; P	-1.00614	-1.03261	-1.00508	-1.00429	-1.00366	-1.00276	-1.00157	-1.00101	-1.00021
GP, CAL/(G) (K)	1.0238	1.0700	1.105.	1.0904	1.0786	1.0611	1.0364	1.0242	1.0173
GAMMA (S)	0.6142	0.5393	0.5888	0.5680	0.5509	0.5245	0.4949	0.4636	0.4507
SON VEL, M/SEC	1.1605	1.1784	1.1713	1.1740	1.1765	1.1810	1.1892	1.1925	1.2074
MACH NUMBER	1.085.6	1.055.7	1.072.6	1.061.7	1.052.3	1.036.6	1.007.5	987.0	970.6
VELC, FT/SEC	0.00	1.00	0.562	0.767	0.910	1.112	1.419	1.610	1.749
VISC, G/CH-SEC	.000606	.000666	.000895	.000884	.000874	.000856	.000824	.000799	.000779
C, CAL/G-SEC-K	.000291	.000276	.000287	.000283	.000285	.000274	.000265	.000252	.000235
I, CV, DEC K	3/153	3/153	3/153	3/153	3/153	3/153	3/153	3/153	3/153
IMPETUS	394 x 0.								
CONSTANT, FT/SEC									
CF	.670	.386	.521	.613	.739	1.016	1.088	1.267	1.589
A/EAT	1.003	1.253	1.008	1.008	1.021	1.198	1.315	1.683	2.265
IVAC,LB-SEC/LB	197.1	227.7	203.8	197.9	198.0	206.7	214.4	228.3	237.7
I, LB-SEC/LD	106.6	61.4	83.0	97.6	117.6	145.6	162.0	173.1	201.7

TABLE IX. Concluded

## MOLE FRACTION

	C0	C2H2	CH	CH2	CH3	CH4	CN	CN2	C2	C3H
	C02	NH	C2H4	C2N	C2O	C3	N2	N2O	H2O	N
CO	.27606	.27371	.27656	.27535	.27438	.27285	.27035	.26867	.26735	.26277
H	.22193	.22587	.22157	.22344	.22316	.22727	.23064	.22583	.22343	.21613
HCO	.00427	.00268	.00382	.00342	.00312	.00260	.00168	.00134	.00181	.00081
H2O	.288016	.000009	.260013	.00812	.00913	.00506	.00005	.00004	.00013	.00001
H2	.00001	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000
H2O	.04746	.04847	.04769	.04795	.04824	.04803	.05026	.05156	.05272	.05721
NH2	.28839	.29217	.28987	.28993	.29170	.29268	.29347	.29339	.29279	.28943
NH3	.00001	.00000	.00001	.00000	.00000	.00000	.00000	.00000	.00000	.00000
NO	.000243	.0001	.00001	.00001	.00001	.00000	.00000	.00000	.00000	.00000
N2	.00195	.00146	.00133	.00160	.00133	.00095	.00046	.00027	.00017	.00000
O	.16733	.14670	.14784	.14822	.14851	.14893	.14946	.14973	.14967	.15006
OH	.000258	.00022	.00004	.00034	.00026	.00017	.00007	.00003	.00002	.00001
O2	.01079	.39607	.00911	.00760	.00676	.00521	.00303	.00195	.00154	.00034
	.000140	.000054	.00106	.00132	.00064	.00042	.00016	.00008	.00004	.00000

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN .000005 FOR ALL ASSUMED CONDITIONS

C	C(S)	CH	CH2	CH3	CH4	CN	CN2	C2	C3H
C2H2	C2H4	C2N	C2O	C3	N2	N2O	N2O(C)	H2O(C)	N
NH	NH	N2C	N2O	N2	N2O	N2O4			

NOTE. MEAN "FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS

VISCOSITY AND CONDUCTIVITY VALUES BASED ON 96.0 PERCENT OF GAS MIXTURE

TABLE X. OUTPUT FOR CASE 102, HMX-RUBBER

## THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING EQUILIBRIUM COMPOSITION DURING EXPANSION

CASE 102 PROPELLANT IS HMX-RUBBER		CHEMICAL FORMULA		WT FRACTION		ENTHALPY		STATE		TEMP		DENSITY		
OXIDANT C	4.00000	H	6.00000	O	6.00000	N	8.00000	(SEE NOTE)	CAL/MOL	DEG K	G/CC			
FUEL C	7.00000	H	11.00000	O	2.00000	N	.02000	1.00000	17900.000	298.00	-9.0000			
O/F =	5.6667	PERCENT FUEL =	15.0000	EQUIVALENCE RATIO =	2.7550	DENSITY =	9.0000							
P/C/P		CHAMBER	THROAT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	EXIT	68.000		
P., ATM	1.000	1.619	1.200	1.400	1.60	2.00	3.00	4.000	5.000	6.000	7.000			
T., CP. DEG K	340.2	187.0	263.5	243.0	212.6	170.1	113.4	65.06	60.56	56.02	51.03			
H <sup>2</sup> , TATE/G		1995	1758	1918	1856	1905	1724	1592	1510	1453	1318	1070		
S., CAL/(G) (K)	43.0	73.8	5.3	24.2	49.8	91.0	160.9	207.0	241.0	337.6	557.9			
H <sub>2</sub> , MOL WT	18.902	19.005	18.925	18.950	18.976	19.030	19.163	19.264	19.392	19.796	21.091			
(OLV/DLP) T	-1.01476	-1.02159	-1.01644	-1.01815	-1.01982	-1.02299	-1.02975	-1.03507	-1.03932	-1.05817	-1.07938			
(OLV/DLP) P	1.0946	1.1603	1.1127	1.1309	1.1469	1.1639	1.2631	1.3303	1.3876	1.4366	2.0465			
CP, TATE/G(K)	533.0	5921	5452	5607	5769	6103	6929	7693	8383	1.3712	2.3570			
GAMMA (S)	1.2863	1.2791	1.2854	1.2837	1.2817	1.2769	1.2642	1.2531	1.2438	1.203	1.1394			
SON VEL, M/SEC	1062.5	991.7	1040.6	1022.5	1006.7	980.7	934.5	903.3	880.2	809.5	693.6			
MACH NUMBER	0.000	1.000	.538	.738	.379	1.083	1.400	1.604	1.754	2.208	3.273			
VEL. FT/SEC	0.0	3253.6	1837.3	2676.8	2903.8	3484.2	4293.7	4752.8	5065.5	5462.3	7361.3			
VISC, G/CM-SEC	0.00604	0.000555	.000576	.000565	.000568	.000521	.000504	.000493	.000469	.000416				
C, TATE/G-SEC-K	0.00391	0.000357	.000380	.000371	.000364	.000351	.000331	.000317	.000307	.000285	.000249			
T, CY, DEG K	2566	377584.												
IMPEXUS														
CSIR, FT/SEC		4627	4627	4627	4627	4627	4627	4627	4627	4627	4627	4627		
CF		.703	.397	.535	.628	.753	.928	1.027	1.095	1.267	1.591			
AR/TAT		1.000	1.239	1.072	1.029	1.006	1.023	1.273	1.631	2.104	2.907			
IVAC/LB-SEC/LB		180.2	210.6	167.0	181.4	160.6	187.3	193.6	198.6	213.6	248.0			
I, LC-SEC/L3		101.1	37.1	76.9	90.3	108.3	133.5	147.7	157.4	182.2	228.8			

TABLE X. Concluded

MOLE FRACTIONS

C(S)	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
CH <sub>3</sub>	.00003	.00001	.00002	.00002	.00001	.00001	.00001	.00001	.00000	.00000	.00000
CH <sub>4</sub>	.00418	.00735	.00494	.00571	.00649	.00605	.00175	.01508	.01603	.00800	.00000
CO	.00082	.00490	.00640	.00595	.00546	.00443	.00181	.03392	.02372	.02120	
CO <sub>2</sub>	.00566	.00741	.00608	.00650	.00693	.00780	.00992	.01194	.01263	.02277	.07542
C <sub>2</sub> H <sub>2</sub>	.00002	.00001	.00002	.00001	.00001	.00001	.00000	.00000	.00000	.00000	
C <sub>2</sub> H <sub>4</sub>	.00002	.00001	.00001	.00001	.00001	.00001	.00000	.00000	.00000	.00000	
H	.00005	.00001	.00003	.00002	.00001	.00001	.00001	.00001	.00001	.00001	
HCN	.00136	.00074	.00114	.00098	.00095	.00067	.00043	.00030	.00023	.00010	.00000
HCO	.00007	.00002	.00005	.00004	.00003	.00002	.00002	.00000	.00000	.00000	
H <sub>2</sub>	.34336	.33876	.34237	.34127	.34059	.33764	.33162	.32616	.32141	.30765	.00000
H <sub>2</sub> O	.02245	.02240	.02165	.02165	.02210	.02266	.02423	.02545	.02656	.03329	.20640
NH <sub>3</sub>	.00065	.00056	.00062	.00060	.00057	.00054	.00049	.00045	.00042	.00033	.05793
N <sub>2</sub>	.71627	.21782	.21706	.21704	.21742	.21814	.21982	.22129	.22259	.22510	.22486

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN .009005 FOR ALL ASSIGNED CONDITIONS

C	CH	CH <sub>2</sub>	CN	CN <sub>2</sub>	C <sub>2</sub>	C <sub>2</sub> H	C <sub>2</sub> N	C <sub>2</sub> N <sub>2</sub>	C <sub>2</sub> O	
C <sub>3</sub>										
N <sub>2</sub> H <sub>4</sub>										

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS  
VISCOSITY AND CONDUCTIVITY VALUES BASED ON 99.4 PERCENT OF GAS MIXTURE

TABLE XI. OUTPUT FOR CASE 106, RDX-TRIAMINO GUANIDINE NITRATE

THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING EQUILIBRIUM COMPOSITION DURING EXPANSION

PC = 50000.0 PSIA

CASE 106 PROPELLANT IS ROX-TAG NITRATE

CHEMICAL FORMULA						
FUEL	C 2.00000	H 5.00000	O 1.00000	N 3.00000		
FUEL	C 4.00000	H 6.00000	N 4.00000			
OXIDANT	C 3.00000	H 6.00000	O 6.00000	N 6.00000		
OXIDANT	C 1.00000	H 9.00000	O 3.00000	N 7.00000		

Q/F= 2.33333 PERCENT FUEL= 30.0000 EQUIVALENCE RATIO= 2.6026 DENSITY= 0.0000

P/P	CHAMBER	THROAT	EXIT		EXIT	EXIT	DENSITY						
			1.000	1.000									
P, ATM	340.2	186.4	263.5	243.3	212.6	170.1	113.4	86.5	66.5	54.02	5.003		
T, CP, DEG K	2051	1795	1970	1904	1848	1759	1610	1517	1451	1285	2019		
H, CAL/G	9.5	-24.9	58.7	27.1	5.6	-42.0	-114.2	-161.6	-196.4	-294.	-513.2		
S, CAL/(G) (K)	2.5466	2.5166	2.5166	2.5166	2.5166	2.5166	2.5166	2.5166	2.5166	2.5166	2.5166		
M, MOLE WT	18.760	18.777	18.763	18.766	18.777	18.783	18.823	18.875	18.934	19.227	20.343		
(DLV/DLP) T	-1.00316	-1.00507	-1.00350	-1.00393	-1.00443	-1.00561	-1.00643	-1.01395	-1.01859	-1.03637	-1.07293		
(DLV/DLT) P	1.0171	1.0359	1.0257	1.0249	1.0297	1.0412	1.0794	1.1274	1.1795	1.2036	1.2373		
CP, CAL/(G) (K)	4.866	4.656	4.671	4.887	4.914	4.995	5.338	5.633	6.613	9.227	2.2561		
GAMMA (S)	1.2855	1.2888	1.2871	1.2861	1.2886	1.2886	1.2886	1.2887	1.2776	1.2694	1.2264		
SON VEL, M/SEC	1081.0	1012.0	1063.0	1042.3	1027.0	1001.7	95.6	92.7	91.5	87.6	87.6		
WACH NUMBER	0.000	1.000	0.538	0.737	0.877	1.079	1.393	1.796	1.777	2.129	3.238		
VEL, FT/SEC	0.0	3320.3	1870.0	2518.8	2955.1	3565.2	4366.5	4636.7	5144.6	5944.9	7416.6		
VISC, G/CM-SEC	0.000624	0.000568	0.000656	0.000592	0.000580	0.000582	0.000528	0.000508	0.000493	0.000460	0.000397		
L, LAL/G-SEC-K	.000461	.000366	.000390	.000361	.000374	.000361	.000343	.000326	.000316	.000289	.000234		
T, CV, DEG K	2637	3908.0											
IMPELUS													
CSSTAR, FT/SEC	4704	4704	4704	4704	4704	4704	4704	4704	4704	4704	4704		
CF	.706	.338	.336	.629	.794	.928	1.027	1.034	1.034	1.264	1.577		
A/E/AT	1.000	1.282	1.073	1.014	1.005	1.118	1.266	1.417	2.139	2.139	8.693		
IVAC,LB-SEC/LB	183.3	214.3	190.3	184.3	185.7	190.2	196.4	201.3	210.1	249.2	230.5		
I, LB-SEC/LB	103.2	58.1	78.3	91.6	110.2	135.7	150.1	159.9	184.8				

TABLE XI. Concluded

## MOLE FRACTIONS

ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MOLE FRACTIONS WERE LESS THAN .00005 FOR ALL ASSIGNED CONDITIONS

ON 20 40 0 402N 02N 4024 32N 20N  
NH 2HN HN N (S)02H (1)02H 20H C3 C2C 2NC  
NH3O 3H3O H3O O 20 240 N2 CH2C H2C C

NOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXIDANT IN TOTAL OXIDANTS.

### WISCOSE AND CONDUCTIVITY VARIATIONS BASED ON 99.8 PERCENT OF GAS MIXTURE

TABLE XII. THERMO DATA INPUT FORMAT FOR TITANIUM DIOXIDE

		TITANIUM DIOXIDE (TiO <sub>2</sub> ) IDEAL GAS			
-62000.0	9.51				
298 300	400 500	600	700 800	900 1000	
10.838	10.858	11.820	12.548	13.079	13.464
0.000	•020	1•156	2•376	3•659	4•987
56.146	56.213	59.474	62.194	64.531	66.578
10001100120013001400150016001700180019002000210022002300240025002600270028002900					
20003100320033003400350036003700380039004000410042004300440045004600470048004900					
500051•520053005400550056005700580059006000					
14.117	14.117	14.339	14.417	14.480	14.532
14.690	14.709	14.725	14.741	14.754	14.765
14.807	14.813	14.819	14.824	14.828	14.832
14.849	14.852	14.854	14.856	14.858	14.860
14.869	14.870	14.871	14.872	14.874	14.875
14.879					
9.138	10.556	11.985	13.423	14.868	16.319
23.630	25.099	26.571	28.045	29.519	30.995
38.389	39.570	41.352	42.834	44.317	45.800
53.220	54.705	56.191	57.676	59.162	60.648
68.080	69.567	71.054	72.541	74.029	75.516
62.955					
71.506	72.858	74.101	75.252	76.323	77.324
81.529	82.246	82.931	83.586	84.213	84.816
87.512	87.997	88.468	88.924	89.336	89.796
91.778	92.145	92.503	92.852	93.194	93.523
95.094	95.383	95.677	95.960	96.238	96.511
97.806					

TABLE XIII. THERMØ DATA OUTPUT FORMAT FOR TITANIUM DIOXIDE

TITANIUM DIOXIDE (TiO<sub>2</sub>) IDEAL GAS

H0 = -62000.0

VALUES OF G COEFFICIENTS ARE									
T	CP	CCP	HT	CHT	ST	GST	DCP	DHT	DST
298.	10.838	10.838	0.000	0.100	56.146	56.146	.006	0.000	.000
300.	10.850	10.850	-0.020	-0.022	56.213	56.213	.002	.002	.006
400.	11.820	11.816	1.156	1.158	59.474	59.480	.004	.002	.006
500.	12.546	12.540	2.376	2.377	62.194	62.198	.008	.001	.004
600.	13.879	13.076	3.659	3.659	64.531	64.534	.003	.000	.003
700.	13.464	13.465	4.987	4.987	66.578	66.581	.001	.000	.003
800.	13.746	13.746	6.346	6.349	68.395	68.398	.000	.001	.003
900.	13.957	13.952	7.734	7.734	70.027	70.030	.004	.000	.002
1000.	14.117	14.118	9.138	9.138	71.506	71.509	.001	.000	.003
VALUES OF G COEFFICIENTS ARE									
1000.	14.117	14.117	9.138	9.138	71.506	71.506	.000	.000	.000
1100.	14.261	14.214	18.556	18.555	72.858	72.856	.027	.001	.002
1200.	14.339	14.301	11.981	11.981	74.101	74.097	.038	.004	.004
1300.	14.447	14.379	17.423	17.415	75.252	75.245	.038	.008	.002
1400.	14.480	14.447	14.668	14.856	76.323	76.313	.033	.012	.010
1500.	14.532	14.508	16.319	16.304	77.324	77.312	.024	.015	.012
1600.	14.575	14.561	17.774	17.757	78.263	78.250	.014	.017	.013
1700.	14.611	14.607	19.234	19.216	79.147	79.134	.004	.018	.013
1800.	14.641	14.646	20.696	20.678	79.948	79.970	.005	.018	.022
1900.	14.667	14.681	22.162	22.145	80.276	80.263	.014	.017	.013
2000.	14.698	14.709	23.630	23.614	81.529	81.516	.019	.016	.013
2100.	14.709	14.734	25.099	25.186	82.246	82.235	.025	.013	.011
2200.	14.726	14.754	26.571	26.561	82.931	82.921	.028	.010	.010
2300.	14.741	14.771	28.045	28.037	83.586	83.577	.030	.008	.009
2400.	14.754	14.784	29.515	29.515	84.213	84.206	.030	.004	.007
2500.	14.766	14.795	30.985	30.984	84.816	84.809	.036	.001	.002
2600.	14.776	14.803	32.472	32.474	85.395	85.390	.027	.002	.005
2700.	14.785	14.808	33.980	33.984	85.953	85.949	.024	.004	.006
2800.	14.793	14.814	35.429	35.435	86.491	86.487	.021	.006	.004
2900.	14.808	14.817	36.989	36.917	87.010	87.007	.017	.008	.003
3000.	14.807	14.819	38.389	38.399	87.512	87.510	.012	.010	.002
3100.	14.813	14.821	39.870	39.881	87.997	87.995	.008	.011	.002
3200.	14.819	14.821	41.352	41.363	88.468	88.466	.002	.011	.002
3300.	14.824	14.822	42.834	42.845	88.924	88.922	.002	.011	.002
3400.	14.828	14.823	44.317	44.327	89.336	89.365	.005	.010	.029
3500.	14.832	14.823	45.804	45.810	89.796	89.794	.009	.010	.002
3600.	14.836	14.824	47.283	47.292	90.214	90.212	.012	.009	.002
3700.	14.840	14.826	48.767	48.775	90.621	90.618	.015	.008	.003
3800.	14.843	14.827	50.251	50.257	91.017	91.013	.016	.006	.004
3900.	14.846	14.829	51.736	51.736	91.402	91.399	.017	.004	.003
4000.	14.849	14.832	53.220	53.220	91.778	91.774	.017	.003	.004
4100.	14.852	14.836	54.705	54.706	92.145	92.140	.017	.001	.005
4200.	14.854	14.839	56.191	56.190	92.503	92.498	.015	.001	.005
4300.	14.856	14.844	57.676	57.674	92.852	92.847	.012	.002	.005
4400.	14.858	14.848	59.162	59.159	93.194	93.188	.010	.003	.006
4500.	14.860	14.854	60.644	60.644	93.528	93.522	.006	.001	.006
4600.	14.862	14.859	62.134	62.130	93.854	93.849	.003	.004	.005
4700.	14.864	14.865	63.620	63.616	94.174	94.168	.001	.004	.006
4800.	14.866	14.871	65.107	65.103	94.487	94.481	.005	.004	.006
4900.	14.867	14.876	66.593	66.590	94.794	94.784	.009	.003	.006
5000.	14.869	14.881	68.080	68.078	95.094	95.089	.012	.002	.005
5100.	14.870	14.886	69.567	69.566	95.388	95.383	.016	.001	.005
5200.	14.871	14.889	71.054	71.055	95.677	95.672	.018	.001	.005
5300.	14.872	14.892	72.541	72.544	95.960	95.956	.020	.003	.006
5400.	14.874	14.893	74.029	74.033	96.230	96.235	.019	.004	.003
5500.	14.876	14.892	75.516	75.523	96.511	96.508	.017	.002	.003
5600.	14.876	14.889	77.004	77.012	96.779	96.776	.013	.008	.003
5700.	14.877	14.883	78.491	78.500	97.043	97.040	.006	.009	.003
5800.	14.878	14.875	79.979	79.988	97.301	97.298	.003	.009	.003
5900.	14.878	14.862	81.467	81.475	97.556	97.553	.016	.008	.003
6000.	14.875	14.847	82.955	82.960	97.806	97.802	.032	.005	.006

TABLE XIV. DATA TAPE FORM FOR THERMΦ DATA OUTPUT

T102	J	6/70T1	10	200	000	06	209.000	6000.000		1
C•62406876E+01	0•12846967E-02	-0•50184624E-06	0•85525393E-10	-0•53125222E-14					2	
-0•33336518E+05	-0•81878897E+01	0•30725348E+01	0•10883020E-01	-0•11120307E-04					3	
0•49483359F-08	-0•67934354F-12	-0•32508921E+05	0•79567663F+01						4	

## SECTION V

### THERMO DATA PROGRAM

The program (Appendix II) to fit the tabular JANAF thermochemical data to the Lewis polynomial is relatively simple and straightforward. JANAF data for Cp, H, and S is read in the tabular form for two temperature ranges 298° to 1,000°K and 1,000° to 6,000°K. The format is as shown in Table XII for the gas Ti<sub>0</sub>2. The first line consists of the reference heat of formation to 298°K in calories per mole, the number of points in the first temperature range and the number of points in the second temperature range, followed by a species identifier. The tabular temperature references for the first interval are then listed followed by the appropriate Cp, H, and S values. This sequence is then repeated for the second temperature range. Subsequent to data input, the program establishes a matrix which it solves by an inversion procedure to obtain the required polynomial constants. These constants are then output in the form suitable for inclusion on the Lewis program thermodynamic data tape.

The output is as shown on Table XIII for the Ti<sub>0</sub>2 species which is also shown on the input. The coefficients required on the data card for the first temperature range are shown on the first line followed by a comparison between the tabular data and the generated polynomials for the three functions of interest. It can be seen that the data fit is quite good. These data are followed by the required constants for the second temperature range and a similar comparison of polynomial and tabular results.

These results are read onto the data tape in the form shown on Table XIV. There are four cards per species. The first line consists of the empirical formula in columns 1 to 12. A gaseous species has no subscript, a liquid, has subscript L, and a solid, has subscript S. Columns 19 to 21 contain a code for the data source, in this case, a J for the JANAF tables. Columns 22 to 24 are the month and year of polynomial computation. The first through the fourth atoms in the species are inserted in columns 25 and 26, 30 and 31, 35 and 36, 40 and 41, while the respective number of atoms are placed in columns 27 to 29, 32 to 34, 37 to 39, and 42 to 44. Column 45 is used for the phase of the species G, L, or S. Columns 46 through 55 have the lower temperature bound at which the species exists with the upper temperature bound being placed in columns 56 through 65.

Cards 2, 3, and 4 contain the 14 polynomial constants, five each on cards 2 and 3 and four on card 4.

APPENDIX I  
LEWIS PROGRAM LISTING

35

(The reverse of this page is blank)

PROGRAM P1712 FORTRAN EXTENDED VERSION 2.0 31/12/70 08.09.56. PAGE NO. 1

```

      PROGRAM P1712 INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT,TAPE4,TAPE5
      DATA MIT/4HOMIT/,BLANK/1H /,PSIA/4HPSIA/,REAC/4HREAC/
      1 INPUT/4MINPU/,IE/1HE/,INSERT/4HINSE/,THRM/4HTHER/,END/3HEND/
      2 DATA LH/4HH,CA,4HL/G/,LVM/2HV+,1H /,LVM/2HV-,1H /,NNLT/4HNAME/
      3 NAMELIST/INPT2/JANF,P,T,EQRT,OF,FPGT,FA,TP,HP,SP,RKT
      4 T,PSIA,MMHG,SHOCK,TGNS,EV,V,DETR,CPCVFR,CPCVEQ,TDEBUG
      5 2,SIUNIT,EUITS
      C EQUIVALENCE (ONIT,ENLN),(INSERT,EN(1,3))
      C
      C DATA MIT/4HOMIT/,BLANK/1H /,PSIA/4HPSIA/,REAC/4HREAC/
      1 INPUT/4MINPU/,IE/1HE/,INSERT/4HINSE/,THRM/4HTHER/,END/3HEND/
      2 DATA LH/4HH,CA,4HL/G/,LVM/2HV+,1H /,LVM/2HV-,1H /,NNLT/4HNAME/
      3 NAMELIST/INPT2/JANF,P,T,EQRT,OF,FPGT,FA,TP,HP,SP,RKT
      4 T,PSIA,MMHG,SHOCK,TGNS,EV,V,DETR,CPCVFR,CPCVEQ,TDEBUG
      5 2,SIUNIT,EUITS
      C
      C TLOW = 0.
      C NMR = .FALSE.
      C 00 399 1=1.15
      C -00 -396 -J=1.150
      C
      C A(I,J) = 0.0
      C 398 CONTINUE
      C 399 CONTINUE
      C
  
```

```

PROGRAM F1712 FORTRAN EXTENDED VERSION 2.0
31/12/70 00.0956.

      1  WRITE(*,*)  

      55   400 FORMAT(1H1)  

           R24(5.12,0) NREAC,NCASE,NSRIT,NMHT  

     120.  FORMAT(1H1)  

           IF(NREAC.LE.0.OR.NCASE.LE.0) WRITE(6,1023) NREAC,NCASE  

     1023 FORMAT(1H*,*NO REACTANTS OR NO CASES SPECIFIED ON TYPE 1 DATA CARD P1712  

           NMHT=1,NCASE=1,I3,*  

     60      11 NMHT = 0  

           NSRIT = 0  

           MOLES = .FALSE.  

           CALL REACT  

           IF(L.EQ.0) WRITE(6,52)  

     52      5- FORMATTED-ERROR-I-REACTANT-CARDS  

           C  CHECK INSERT CARDS  

           C  IF (INSRT.LE.0) GO TO 205  

     70      180  DO 185 K=1,NSRIT  

           READ(5,205) TOTAT(J,J=1,15)  

           WRITE(6,205) (DATA(J),J=1,15)  

     204  FORMAT(5I3A4,3X)  

     2045 2045 (IX,5I3A4,3X)  

     185  DO 185 J=1,15,3  

           IF (DATA(J).EQ.BLANK) GO TO 185  

           185 CONTINUE  

           C  INSERT - NSRIT+1  

           INSERT(1,NSRIT) = DATA(1)  

           INSERT(2,NSRIT) = DATA(I+1)  

           INSERT(3,NSRIT) = DATA(I+2)  

     38      105 CONTINUE  

           C  CHECK OMIT CARDS  

     5      C  205 IF (NMHT.LT.0) GO TO 210  

           DO 208 K=1,NMHT  

           READ(5,204) (DATA(J),J=1,15)  

           WRITE(6,205) (DATA(J),J=1,15)  

     208  DO 208 J=1,15,3  

           IF (DATA(J).EQ.BLANK) GO TO 208  

           NMHT = NMHT+1  

           OMIT(1,NMHT) = DATA(I)  

           OMIT(2,NMHT) = DATA(I+1)  

           OMIT(3,NMHT) = DATA(I+2)  

     95      208 CONTINUE  

           NEUR=.TRUE.  

           C  BEGIN NAMELIST INPT2  

     100    C  210 DC 500 NC5=1,NCASE  

           DO 344 I=1,24  

           CCP(I) = 0.  

           T(I) = 0.  

           V(I) = 0.  

     105    C

```

```

PROGRAM P1712 FORTRAN EXTENDED VERSION 2.0      31/12/70      08.09.56.
----- 300 CONTINUE
      V1 = 0.
      V2 = 0.
      RHOP = 0.
      KASE = 0
      TP = .FALSE.
      HY = .FALSE.
      SP = .FALSE.
      RKI = .FALSE.
      CPCVFR = .FALSE.
      CPCVEQ = .FALSE.
      SHCK = .FALSE.
      DENTN = .FALSE.
      FV = .FALSE.
      PASCAL = .FALSE.
      MMHG = .FALSE.
      PSIA = .FALSE.
      R = 1.987165
      TTR = 67184.**R
      SIUNIT = .FALSE.
      EUNITS = .FALSE.
      I0NS = .FALSE.
      IDEBUG=.FALSE.
      FA = 0.
      OF = U.
      EQRAT= 0.
      FPCT= 0.
      ECL = .TRUE.
      READ(5,333)KASE
      333 FORMAT(13A6,A2)
      *TTR(5,INPT2)
      DO 305 I=1,26
      IF(P(I).EQ.0.) GO TO 322
      NP = I
      IF (MMHG) P(NP) = P(NP)/760.
      IF (PASCAL) P(NP) = P(NP)/101325.
      IF(TPSTA)=P(TNP7714.596076
      305 CONTINUE
      322 IF (FA.NE.0.) OF = 1./FA
      IF(EQRAT.EQ.0.) GO TO 725
      OF= (-EQRAT*VMN2)-VPLS(2)/(VPLS(1)+EQRAT*VHIN(1))
      GO TO 727
      728 IF(TPSTA)=OF-TPSTA
      145 IF(FPCT.EQ.0.) GO TO 4051
      OF= (1LJ.-FPCT)/FPCT
      GO TO 727
      9051 WRITE(6,724)
      724 FORMAT(4BHNO INPT2 VALUE GIVEN FOR OF, EQRAT, FA, OR FPCT )
      727 IF(TMP7714.596076-OF=TMP7714.596076)
      -155 727 MP(1) = OF
      MP(2) = 1.
      SUM = MP(1)*MP(2)
      FPCT = 100.*MP(2)/SUM

```

```

----- PAGE NO. 3 -----
      P1712 00108
      P1712 00109
      P1712 00110
      P1712 00111
      P1712 00112
      P1712 00113
      P1712 00114
      P1712 00115
      P1712 00116
      P1712 00117
      P1712 00118
      P1712 00119
      P1712 00120
      P1712 00121
      P1712 00122
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      P1712 00155
      P1712 00156
      P1712 00157
      P1712 00158
      P1712 00159
      P1712 00160

```

PROGRAM P1712 FORTRAN EXTENDED VERSION 2.0  
 PAGE NO. 4  
 31/12/70 08.09.56.  
 160 IF (EQRT.EQ.0.) GO TO 746  
 V2 = (WF(1)\*VMIN(1)+F(2)\*VMIN(2))/SUM  
 V1 = (WP(1)\*VPLS(1)+WP(2)\*VPLS(2))/SUM  
 IF (V2.NE.0.) EGRT=ABS(V1/V2)  
 746 DO 747 I=1,L  
 747 S0(I) = (WP(1)\*B0P(I,1)+WP(2)\*B0P(I,2))/SUM  
 IF (EGRT.EQ.1.) EGRT=1.000005  
 IF (NOT.IONS.OR.L.NT(L).EQ.IE) GO TO 748  
 L = L+1  
 LL.PT(L) = IE  
 80(I,I) = 0.  
 748 M3080 = -MPT17+MPP(27\*MPT2)+MPP(27)\*SUM  
 WRITE (6,INPT2)  
 WRITE(6,752)KAST  
 752 FORMAT(1H0,13A6,A2)  
 WRITE (6,770)  
 770 FORMAT(1H0,17X,4HFUEL,13X,7HOXIDANT,12X,7HMIXTURE //)  
 780 FORMAT(1H24\*3E15,77)  
 WRITE (6,790) LH.HPF(2),HPP(1),HSUBG,LVP,VPLS(2),VPLS(1),V1,  
 1LYM,VMIN(2),VMIN(1),V2  
 HSUB0 = HSUB0/R  
 WRITE (6,795)  
 795 FORMAT(8H ATOMS/G )  
 WRITE(6,796)TANK,TB0,TB1,TB2,R0P(T1,T2),R0P(T1,T3),R0P(T1,T4)  
 185 RHJP = HP(2)\*RH0(1)\*HP(1)\*RH0(2)  
 IF (RH0.NE.0.) RNCP = (WP(1)+WP(2))\*RH0(1)\*RHC(2)/RH0P  
 40 796 IF (NEAR) CALL SEARCH  
 \*01= 1,\*1  
 IF (INC.EQ.0) GO TO 790  
 790 DO 302 J=1,N  
 IF (IUSE(J).EQ.0) GO TO 302  
 IF (IUSE(J).GT.0) IUSE(J) = -IUSE(J)  
 IF (INSERT.EQ.0) GO TO 302  
 00 301 I=1,INSERT  
 IF (SUB(J,1).NE.ENSERT(1,1)) GO TO 301  
 -IF (SUB(J,2).NE.ENSERT(2,1)) GO TO 301  
 IF (SUB(J,3).NE.ENSERT(3,1)) GO TO 301  
 ENSERT(1,1) = 0.  
 IC1= 101+1  
 IUSE(J) = -IUSE(J)  
 200 301 CONTINUE  
 302 CONTINUE  
 ENH  
 210 SUPN = ENN  
 XI = NS - NC  
 XI = ENM/XI  
 XLH = A1.9G(XI)  
 205

PROGRAM P1712 FORTRAN EXTENDED VERSION 2.0  
 31/12/70  
 PAGE NO. 5  
 08.09.56.  
 215  
 432 J=I,N  
 IF (IUSE(J) .EQ. -10000) IUSE(J)=0  
 EN(L,J,1) = 0.  
 ENLN(J)=0.  
 IF (IUSE(J) .NE. 0) GO TO 432  
 EN(L,J,1) = XI  
 EN(L,J,2) = XLN  
 220 432 CONTINUE  
 JSCL = 0  
 JLIQ = 0  
 IF (DETM) CALL DETON  
 IF (RK1) CALL ROCKET  
 IF (TP) CALL MOLIER  
 225 500 CONTINUE  
 GO TO 1  
 END  
 -----

P1712 00214  
 P1712 00215  
 P1712 00216  
 P1712 00217  
 P1712 00218  
 P1712 00219  
 P1712 00220  
 P1712 00221  
 P1712 00222  
 P1712 00223  
 P1712 00224  
 P1712 00225  
 P1712 00226  
 P1712 00227  
 P1712 00228  
 P1712 00229  
 P1712 00230  
 -----

BLOCK DATA

FORTRAN EXTENDED VERSION 2.0

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08.09.56.



ROUTINE CHSTN FORTRAN EXTENDED VERSION 2.0

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三五九

31/12/2023

THE RAILROAD

二

## FORTRAN EXTENDED VERSION 2.0

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PAGE NO. 1

```

      SUBROUTINE CPHS
COMMON/SPECIES/COEF(2,7,150),S(150),EN(150,13),ENLN(150),HO(150)
1  ,CELN(150),A(15,150),SUB(150,3),IUSE(150),TEN(150,2)
1  ,COMMON/*SCFENN,SUHN,TT,SOATOM(3,101),LLMT(15),BU(15),BOP(15,2)
1  ,TEN,OK,IMID,THIGH,PP,CPSUM,OF,EORA,FPCT,R,ER,HSUB0,AC(2),AM(2)
1  ,TPPT(2),RDPT(2),VMINT(2),VPLST(2),TP(2),DATA(227),NAME(15,5)
2  ,ANUM(15,5),PECWT(15),ENTH(15),FAZ(15),RTEMP(15),FOX(15),DENS(15)
4  ,RHOP,RHM(15),TLN,JANF
COMMON/INDEX/ IDEBUG,CONVG,TIP,HP,SP,HPSp,TPSp,MOLES,NP,NT,NP1,L,NS,
10   P1712 00355
1  ,KMAT,THAT,IQ1,N,J,NOMIT,TIP,NEWR,NSUB,NSUP,IIN,CPGVFR,CPGVEO
1  ,IONS,IC,INSERT,JSOL,JIQ,KASE(14),NREAC,IC,IQ2
1  ,P1712 00363
1  ,P1712 00364
1  ,P1712 00365
1  ,P1712 00366
1  ,P1712 00367
1  ,P1712 00368
1  ,P1712 00369
1  ,P1712 00370
1  ,P1712 00371
1  ,P1712 00372
1  ,P1712 00373
1  ,P1712 00374
1  ,P1712 00375
1  ,P1712 00376
1  ,P1712 00377
1  ,P1712 00378
1  ,P1712 00379
1  ,P1712 00380
1  ,P1712 00381
1  ,P1712 00382
1  ,P1712 00383
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1  ,P1712 00394
1  ,P1712 00395
1  ,P1712 00396
1  ,P1712 00397
1  ,P1712 00398
1  ,P1712 00399
1  ,P1712 00400
      K = 1
      IF(NT,LF,1M1D)K = 2
      KK = 0
      CPSUM=0.
      90 IF(COEF(K,1,J)*NE.0.)GO TO 97
      97 IF(CIUSE(TJ,LT,UT,GT,LT,UT)KK = K
      K = 1
      IF(IKK.EQ.1) K = 2
      IF(IJANF.EQ.0)GO 10 98
      98 CONTINUE
      IF(IJANF.EQ.0)GO 10 98
      1  ,STJ*COEF(TK,TJ).TEN*COEF(TK,TJ)=COEFTK,5,TTTZ,TTTT
      1  +(COEF(K,4,J)/3.0*TT+COEF(K,3,J)/2.0)*TT+COEF(K,2,J)*TT
      1  +HO(J=((COEF(K,"J)/4.0)*TT+COEF(K,3,J)/3.0)*TT+COEF(K,2,J)/2.0)*
      1  TT+COEF(K,1,J)-(COEF(K,5,J)/TT+COEF(K,6,J))/TT
      1  ,CPSUM=CPSUM+((COEF(K,4,J)*TT+COEF(K,3,J))*TT+COEF(K,2,J))*TT
      1  +COEF(K,1,J)*TT+COEF(K,5,J)/TT+COEF(K,4,J)*TT+COEF(K,3,J)*TT
      1  +COEF(K,1,J)/TT+EN(J,NPT)
      30  GO TO 99
      99 S(J) = (((COEF(K,5,J)/4.0)*TT+COEF(K,4,J)/3.0*TT+
      1  ,TT+COEF(K,2,J))*TT+COEF(K,1,J)*TLN+COEF(K,7,J)
      1  ,HU(J) = (((COEF(K,5,J)/5.0)*TT+COEF(K,4,J)/4.0*TT+
      1  ,TT+COEF(K,2,J)/2.0)*TT+COEF(K,1,J)+COEF(K,6,J)/TT
      1  ,CPSUM= CPSUM+(((COEF(K,5,J)*TT+COEF(K,4,J))/TT+COEF(K,3,J)*TT
      1  +COEFTK,TJ,TT+COEFTK,TJ,TT+COEFTK,TJ,TT+COEFTK,TJ,TT)*EN(J,NPT))
      40  99 CONTINUE
      IF(IKK.F0.0) G 10 10U
      K = KK
      KK = 0
      100 IF(J,E0,NS) GO TO 200
      200 RETURN
      ENC
      45

```

```

      C   SUBROUTINE DETON          P1712 00401
      C
      C   CHAPMAN-JOUQUET DETONATIONS          P1712 00402
      05  C   LOGICAL HP,SP,TF,IOEBUG,HEMR,IONS,MOLES,FROZ,EGL,PSIA,RKT          P1712 00403
      C   LOGICAL CPCVFR,CALCH          P1712 00404
      C
      DIMENSION GM(13),CP(13),H1(13),H2(13),PUA(13),TUB(13),GM1(13),RRHO(13)          P1712 00405
      C
      COMMON/POINTS/HSUM(13),SSUM(13),CPR(13),OLYTP(13),DLVPT(13),
      *GAMMAS(13),P(26),T(26),V(13),PPP(13),WM(13),SONVEL(13),FTT(13)          P1712 00406
      C
      *TOTNT13          P1712 00407
      COMMON/SPECIES/COEF(2,7,150),S(150),EN(150,1,3),ENL(150),HO(150)
      1  *CELN(150),A(15,150),SUB(150,3),IUSL(150),TEMP(50,2)          P1712 00408
      C
      CJOHN/MISCELLANEOUS,IT,S,ATOM(3,1U1),LLM(15),BOP(15,2)
      1  *TM TLOA,TMID,THIGH,PP,C?SUM,EGRAT,EPCT,R,RR,HSUB0,AC(2),AH(2)          P1712 00409
      2  *HPP(2),RH0(2),VMIN(2),VPLS(2),MP(2),DATA(22),NAME(15,5)          P1712 00410
      3  *TRDMT15,STPECNT,TST,ENTHT15,FTZ(LIST,RTEMPTY),FDX(LST,DENST15)          P1712 00411
      20  *RH0P,R4W15),TLN,JANF          P1712 00412
      CCOMMON/CUTP/FT(30),FP(4),FT(4),FH(4),FS(4),FM(4),FV(4),FO(4)
      1  *KMAT,IA1,IQ1,N,J,NOINIT,IP,NEWR,NSUP,IN,CGCVFR,CGCVQ          P1712 00413
      2  *IONS,NC,INSERT,JSOL,ULIQ,KASE(14),NREAC,IC,IQ2          P1712 00414
      COMMON/FER/FCP(26),VMOC(13),SPIM(13),VACI(13),SUBAR(13),SUPAR(13)          P1712 00415
      C
      *CPFFT15,ATAT(13),CUSTK,EDLT,FR0Z,SSU          P1712 00416
      C
      C
      46  *MON/CUTP/FT(30),FP(4),FT(4),FH(4),FS(4),FM(4),FV(4),FO(4)
      1  *FC(4),FG(4),FB,FMT13,F1,F2,F3,F4,F5,F6,F7,F8,F9,F10,F11,F12          P1712 00417
      2  *FR1,FC1,FM(4),F2(4),F1(4),F1(4),F1(4),F1(4),F1(4),F0          P1712 00418
      30  C
      EQUIVALENCE(CP,DATA),(GM,SP14),(H1,VACI),(PUB,SUBAR),(TUB,SUPAR)          P1712 00419
      C
      EQUIVALENCE(GM,REALTY),(PCP14,T,RRHO)          P1712 00420
      C
      DATA FT1/4HT1,0/, FP1/4HP1,A/, FH1/4HH1,C/, FM1/4HH1,M/
      1  * FC1/4HCP1,/, FG1/4HA1,/, FPP/4HP/P/, FTT/4HT/T1/
      2  * FUG/4HDT/, FMM/4HR,M1/, FRA/4HRHD/, FRE/4HRHD1/
      3  * FMA/4HACH/, FM3/4H NO/, IZERO/2H00/          P1712 00421
      C
      35  C
      0(G)= A11*A22-A21*A12
      XX(1)=(B1*A22-E2*A12)/D(G)
      YY(2)=(B2*A11-E1*A21)/D(G)
      DO 2 N=1,NREAC
      IF(NAME(N,5).EQ.IZERO) CALCH=.TRUE.
      NT = 1
      NSUB0 = NSUB0+R
      CALCH=.TRUE.
      TT = 0.
      IF(T(1).EQ.0.) T(1)=RTEMP(1)
      DO 2 N=1,NREAC
      IF(NAME(N,5).EQ.IZERO) CALCH=.TRUE.
      2 CONTINUE
      0C 3 IT = 1,26
      IF (T(1)).EQ.0.) GO TO 7
      NT = IT
      3 CONTINUE
      P1712 00422
      P1712 00423
      P1712 00424
      P1712 00425
      P1712 00426
      P1712 00427
      P1712 00428
      P1712 00429
      P1712 00430
      P1712 00431
      P1712 00432
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      P1712 00434
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      P1712 00438
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      P1712 00440
      P1712 00441
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      P1712 00445
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      P1712 00499
      P1712 00500
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```

## SUBROUTINE DETON FORTRAN EXTENDED VERSTON 2.0

31/12/70

08.09.56. -- PAGE NO. 2

```

      7 IF(TAH(1)*NE.0.C-.AM(2).NE.0.D) GO TO 4
      55 AM1 = AM(2)
      IF (AM(2).EQ.0.0) AM1 = AM(1)
      GC TO 9
      4 AM1 = (WP(1)+WP(2))*AM(1)*AM(2)/(WP(1)+WP(2))*AM(1)+AM(2)
      3 CONTINUE
      60 DO 902 TT=1,NT
      T1= TT
      TT = 1
      IF ('QALCH') CALL HCALC
      CP1 = (WP(1)*AC(1)+WP(2)*AC(2))/(WP(1)+WP(2))
      65 DO 902 IP=1,NP
      P1= P+IP
      H1(NP,1) = HSUB0
      TUB(NP,1)=T1
      PUP(NP,1)=P1
      CP(NP,1) = CP1*Q
      ITR= 0
      TT= 3000.
      PP1= 15.
      PP2= PP1*P1
      HSUB0 = H1(NP,1)/R + .75*T1*PP1/AM1
      70 TP = .FALSE.
      HP= .TRUE.
      CALL EOLDRM
      HSUB0 = H1(NP,1)
      HP= .FALSE.
      IF (TT.EQ.0.) GO TO 1000
      GA= GAMMAS(NP,1)
      T1= TT/T1
      TT= 0
      85 TEM=TT1-.75*PP1/(GPR(NP,1)*AM1)
      AMH=WM(NP,1)/AM1
      IF (IDEBUG) WRITE(6,190)
      190 FORMAT(33H1DETONATION VELOCITY CALCULATIONS /11X,4HP/P1,17X,4HT/1
      1)
      98 C 200 DO 202 II=1,4
      ALFA=AMM/TT1
      PP1= (1.+GAH)*(1.+(1.-b.*GAH*ALFA)/(1.+GAH)**2)**5)/(2.*GAH**LFA)
      RK=PP1*ALFA
      TT=TEM+.5*PP1*GAH*(RK*RK-1.)/(AM1*GPR(NP,1)*RK)
      202 FORMAT(15,2E20.8)
      203 CONTINUE
      100 TP= .TRUE.
      TT= T1*TT1
      RR4= -PP1*AMM/TT1
      105 C 205 IT=q ITR+1
      PP= P1+PD1
      CALL EOLDRM

```



## SUBROUTINE DETON FORTRAN EXTENDED VERSION 2.0

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```

160      X2 = YY(2)
        AA = .5*(1.-OLVPT(NPT))
        BB = .5*OLVPP(NPT)
        UD = UD*(AA*X1+BB*X2-1.)
        X1 = X1-1.0
        IF(IODEBUG) WRITE(6,81) X1,X2,UD
        81 FORMATTED T3MCNP AT TT,MT,GT1H=3E17.81
        B1= GAM*RR1
        B2= -81*RR1*MM(NPT)*CP(NPT)/(R*T1)
        X1 = XX(Y)
        X2 = YY(Z)
        UD= UC*(AA*X1+BB*X2+1.)
        X2 = X2-1.
        IF(IODEBUG) WRITE(6,84) X1,X2,UD
        84 FORMAT(6X,16HMT1 AT P1,M1,M1,3X,1H=3E17.81)
        B1= 0.
        B2= -MM(NPT)/(R*T1)
        X1 = XX(Y)*1000.
        X2 = YY(Z)*1000.
        UD= UD*AA*X1+BB*X2)
        IF(IODEBUG) WRITE(6,85) X1,X2,UD
        85 FORMAT(6X,2DHM1 AT T1,P1,M1 =3E17.8)
        C 150 K = 0
        IF(TP>0.ND.TP>0.NT>0.NT>0.EQ.0.1) GO TO 680
        K = NPT
        IF(NPT.NE.13) GO TO 870
        C OUTPUT
        C
        C 860 WRITE(6,5)
        5 FORMAT(1H1,42X,46HOETONATION PROPERTIES OF AN IDEAL REACTING GAS )
        CALL OUT1
        WRITE(6,46)
        46 FORMAT(13H UNSURNED GAS//)
        FMT(4)=FMT13
        FMT(5)=FB
        FMT(7)=F4
        WRITE(E,FMT) FP1,FP(2),FB,(PUB(J),J=1,NPT)
        FMT(7)=F2
        WRITE(6,FMT) FT1,FT(2),FB,F3,(TUB(J),J=1,NPT)
        WRITE(6,FMT) FM1,FM(2),FB,FB,(H1(J),J=1,NPT)
        68-56-1: NPT
        V(I)=AM1
        SORVEL(I) = (RR*GH1(I)*TUB(I)/AH1)**.5
        56 CONTINUE
        FMT(7)=F3
        WRITE(6,FMT) FM1,F4(2)+FM(3),FB,(V(J),J=1,NPT)
        FMT(7)=F4
        WRITE(E,FMT) FC(2),FC(3),FC(4),(CP(J),J=1,NPT)
        WRITE(6,FMT) FG1,FG(1),FG1,FB,FA,(GM1(J),J=1,NPT)
        FMT(7)=F1
        WRITE(E,FMT) FL(I),I=1,4),ISOMVEL(J),J=1,NPT)

```

SUBROUTINE CETON FOFTIAN EXTENDED VERSION 2.0

PAGE NO. 5

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```
      WRITE(6,58)
      58 FORMAT(11HOBURNED GAS//)
      FMT(4)=FMT(6)
      CALL OUT2
      WRITE(6,58)
      68 FORMAT(22HDEUTONATION PARAMETERS //)
      FMT(7)=F7T
      DO 70 I=1,NPT
      V(I)= PGP(I)/PUB(I)
      PCP(I)=ITL(I)/TBL(I)
      SCVEL(I)=SUNVEL(I)*RRHO(I)
      70 CONTINUE
      WRITE(6,FMT)FIT,FB,FB,TV(TJ),J=1,NPT
      WRITE(6,FMT)FB,FB,FB,(PCP(J),J=1,NPY)
      DU 73 I=1,NPT
      V(I)=WM(I)/AM1
      73 CONTINUE
      FMT(7)=F4
      WRITE(6,FMT)FRA,FR3,FS,FB,(RRHO(I),J=1,NPT)
      WRITE(6,FMT)FRA,FR3,FS,FB,(RRHO(I),J=1,NPT)
      WRITE(6,FMT)FMA,FMB,FB,(VKOC(J),J=1,NPT)
      FMT(7)=F1
      WRITE(6,FMT) FUD,FL(2),FL(3),SONVEL(J),J=1,NPT
      E2L=TPUE.
      DATE,OUT3
      865 IF(K.EQ.0) GO TO 1000
      WRITE(6,865)
      865 FORMAT(1M1)
      NPT = 0
      870 NPT = NPT + 1
      5
      C SAVE COMPOSITIONS FOR ESTIMATES OF NEXT POINT
      245 C
      DO 880 I = 1,NS
      EN(Y,NPT) = EN(I,K)
      880 CONTINUE
      902 CONTINUE
      1000 TP = *FALSE.
      RETURN
      END
      250
```

```

C          SUBROUTINE EOLBKM
C          ROUTINE TO CALCULATE EQUILIBRIUM COMPOSITION AND PROPERTIES
C          DOUBLE PRECISION X,G
C          LOGICAL HP,SP,IP,DEBUG,CONVG,IONS,MOLES,FROZ,EQLOGY,HPSPL,TPSP
C          LOGICAL TISINGTTIC
C
C          DIMENSION PROW(18)
C
      05   C          COMMON/POINTS/HSUM(13),SSUM(13),CPR(13),OLVTP(13),OLVPT(13)
           1 ,GAMMAS(13),P(26),T(26),V(13),PPP(13),WM(13),SONVEL(13),TT(13)
           2 ,TTMT(13)
C
      10   C          COMMON/SPECIES/COEF(2,7,150),S(150),EN(150,1,13),ENLN(150)
           1 ,DELN(150),A(15,150),SUB(150,3),IUSE(150),TEMP(150,2)
           2 ,COMMON/MISC/ENN,SUHN,TT,SO,ATOM(3,101),LLMT(15),SU(15),BP(15,2)
           3 ,TM,TLOW,THD,THIGH,WP,CPSUM,OF,EDRAT,FCFT,R,RRHSUB0,AC(12),AH(12),
           4 ,HPP(2),ZHO(2),WHIN(2),VPLS(2),WP(2),DATA(22),NAME(15,5)
           5 ,AMMOMTTS(5),PCHTTS(5),ENTNTTS(5),TAZTTS(5),RTEMP(5),FOXTTS(5),DENSTTS(5)
           6 ,RANP,RHM(15),TLN,JANE
           7 ,COMMON /DOUBLE/ G(20,21),X(20)
           8 ,COMMON/INOX/ IDEBUG,CONVG,TP,HP,SP,HPSPL,TPSP,MOLES,NP,NT,NP+L,NS,
           9 ,KMAT,IMAT,I01,N,J,NOMIT,IP,NEWR,NSUB,NSUP,ITN,CPGCFR,CPGVEQ
          10 ,IONS,NC,NSEKT,JSOL,JLIO,KASE(14),NREAC,IC,IQ2
          11 ,COMMON/PERTPCP/ ZCOT,UMGCTTS(5),SPMTTS(5),VACITTS(5),SUBARTTS(5),SUPARTTS(5)
          12 ,1 ,CPR(13),AEAT(13),CSR,LQL,FROZ,SS0
          13 ,DATA ITER/4HITER/.1E+1HE/,SMALNO/1.E-6/,SMALNO/-13.015511/
          14 ,C          SIZE= 16.5
          15 ,I3HNG,-,PAUSE
          16 ,ENAL = ALOG(ENN),
          17 ,LOGY = .FALSE.,
          18 ,PP_N = ALOG(PP)
          19 ,TLN = ALOG(TT)
          20 ,CONVG = .FALSE..
          21 ,FF4HNG - FFH
          22 ,IF (IC) GO TO 966
          23 ,IF (.NOT. IONS.OR.IE.EQ.0.LLMT(L)) GO TO 10 33
          24 ,L = L+1
          25 ,I01 = I01+1
          26 ,DO 499 J = 1,NS
          27 ,FF-T4T5J,-E8-0.1-68-10-493 -
          28 ,EN(W,NPT) = SMALNO
          29 ,ENLN(J) = SMALNO
          30 ,IUSE(J) = 0
          31 ,499 CONTINUE
          32 ,33 IF(NP).EQ.1 .AND. DEBUG) WRITE(6,244) (LLMT(I),I=1,L),ITER
          34 ,244 FORMAT(1HNP,1H,I4,1H,4T4)
          43 ,TM = ALOG(IP/ENN)
          44 ,J = 1
          45 ,IF(.NOT. IP) CALL CPHS
          46 ,IF(IP.AND.(CONVG.OR.ITNUM3.EQ.1)) CALL CPHS
          47 ,51

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## SUBROUTINE EOL82M FORTRAN EXTENDED VERSION 2.0

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```

      IFTC1J GOTO 171
      IF (.NOT. CONVG.CR. JSOL.EQ.0) GO TO 62
      EN1SOL = EN1JSOL(NPT)
      EN1JSOL(NPT) = EN1JSOL.NPT1 + EN1JL10.NPT)
      USE(JL10) = -USE(JL10)
      IQ1 = IQ1-1

 60   DCVTP(NPT) = 0.
      CP3(NPT) = C.
      GAMMAS(NPT) = 0.
      LOGV = .TRUE.

 62   CALL MATRIX
      NUMB = 1IN-ITNUMB+1
      IF (KOT.CCVG) GO TO 67
      IF (LOGV.AND.JSOL.EQ.0) GO TO 63
      DO 182 I=1,L
      PRCH(I) = G(IQ1,I)
      182 CONTINUE
      IF (.NOT.LOGV) GO TO 67

 63   LCGV = .TRUE.-- SET UP MATRIX TO SOLVE FOR DLVT
      C   63  G(IQ1,IQ2) = ENN
      IG = IQ1 - 1
      DO 777 I = 1,10
      C(I,IQ2) = GT(I,IQ1)

 777 CONTINUE
      67  IF (.NOT.10EBUG) GC TO 72
      WRITE(6,72) NUMB
      772 FORMAT (11H0ITERATION ,I3,6X,7HMATRIX //)
      00 911 I=1,IMAT
      911 WRITE (*,73) IGT,I,KP,I,KMAT)
      72 IF(CCNVG) IMAT=IMAT-1
      ITST = IMAT
      CALL MGAUSD
      IF(ITST.NE.IMAT) GO TO 774
      IF (.NOT.IDEBUG.OR.CCNVG) GO TO 773
      90   WRITE (*,373) ITST,ITST,ITST,ITST
      377 FORMAT (7H0PI ,9HA4.10X)
      WRITE (6,73)(X(I),I=1,IMAT)
      73  COQMAT (9E14,0)
      773 IF (.NOT.CCNVG) GO TO 85
      IF (LOGV) GO TO 171
      95   174 SUM = 0.

      DO 175 J=1,L
      SUM = SUM+PROM(J)*X(J)
      175 CONTINUE
      176  OLVTP(NPT) = 1.+G(I02,IQ1)/ENN-SUM/ENN - X(I01)
      CP4(NPT) = G(I02,I32)
      00 176 J=1,I01
      CP3(NPT) = CPR(NPT)-G(I02,J)*X(J)
      176 CONTINUE
      LOGV = .TRUE.
      GO TO 62

```

## SUBROUTINE EQLBRN FORTRAN EXTENDED VERSION 2.0

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```

C SINGULAR MATRIX          P1712 00759
C                                     P1712 00760
110   774 IF (.NOT.CONVG) GO TO 775      P1712 00761
      WRITE(6,172)                         P1712 00762
      172 FORMAT(25HDERIVATIVE MATRIX SINGULAR )
      IC = .TRUE.
      GO TO 171
115   775 IF (.NOT.HP.OR.NPT.NE.1.OR.NC.EQ.0.OR.TT.GT.100.) GO TO 371
      WRITE(6,874)
      874 FORMAT(96HLOW TEMPERATURE IMPLIES CONDENSED SPECIES SHOULD HAVE
      BEEN INCLUDED ON AN INSERT CARD, RESTART ,
      GO TO 873)
120   871 WRITE(6,74)
      74 FORMAT(16H0SINGULAR MATRIX)
      IF (IC) GO TO 973
      IF (ISING) GO TO 937
      NTZERO = 0
      970 DC 970 JJ = 1, NS
      IF (IUSE(IJJ)) S7C = 968 + 967
      967 IF (EN(JJ,NPT).EQ.0.) GO TO 673
      GO TO 969
      969 IF (EN(JJ,NPT).NE.0.) GO TO 969
      EN(JJ,NPT) = SMALNC
      EN(JJ,J) = -SMALNC
      GO TO 970
      969 NTZERO = NTZERO+1
      970 CONTINUE
      IF (.NOT.IW) GO TO 971
      IC = .FALSE.
      GO TO 43
      971 ISING = .TRUE.
      WRITE(6,776)
      776 FORMAT(1H)RESTART
      GO TO 43
      997 IF (NTZERO.NE.(L-1)) GO TO 873
      IF (TEND.GT.0.0001.DKERRQAT,LT.,0.999999)-GO TO 673
      EN=0.
      NEN = 0
      DO 83 I=1,L
      83 JEN=0
      DO 80 J=1,NS
      IF (TEND.NP+1.EG1.0,GT,6.6-T0-6.0)
      IF (A(I,J).EQ.0.) GO TO 83
      IF (JEN.NE.0) GO TO 83
      JEN = J
      80 CONTINUE
      NEN = NEN+1
      EN=JEN=NPT
      GO TO 43
      43 CONTINUE
      IF (NEN.LT.NTZERO) GO TO 373
      CONVG = .TRUE.
      IC = .TRUE.

```

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SUBROUTINE ECLERM FORTRAN EXTENDED VERSION 2.0
      15      IF(SUM(NPNT)=J) GO TO 84
      16      DO 85 J=1,NS
      17      IF(I(J),NPNT).EQ.0.0) GO TO 84
      18      ENN = EN(J,NPNT)+EN(J)
      19      ENM = EN(J,NPNT)
      20      ENL(J) = ALOG(ENN)
      21      ENSUMPNT = HSUM(PNT) + EN(J,NPNT)*
      22      TM = ALOG(PP/ENN)
      23      GO TO 43
      24      ITNUMB= ITNUMB+1
      25      C-----OBTAIN CORRECTIONS TO THE ESTIMATE
      26      C
      27      KK = L + 1
      28      OLN= X(1102)
      29      IF (TP) JLNT=0.
      30      DO 101 J=1,NS
      31      IF (IUSE(J)) = HO(J)*OLN-HC(J)+S(J)-EN
      32      DELN(J) = HO(J)*OLN-HC(J)+S(J)-EN
      33      DELN(J)= DELN(J)+A(K,J)*X(K)
      34      CONTINUE
      35      GO TO 101
      36      100  DELN(J) = X(100)
      37      KK = KK + 1
      38      101  CONTINUE
      39      AMEDA= 1.
      40      AMDOA1= 1.
      41      SUMP = X(101)
      42      IF ((SUM.LT.0.) .OR. (SUM.GT.0.)) AND (DELN(J).GT.
      43      IFTEN(J).LT.0.) THEN
      44      SUM=DLNT
      45      IF (-OLN.GT.SUM) SUM=-DLNT
      46      00  917  J=1,NS
      47      IF (IUSE(J).NE.0) GO TO 917
      48      IF ((EN(J),NPNT).GT.0.) AND (DELN(J).GT.
      49      IFTEN(J).GT.0.) THEN
      50      SUM1 = (-9.212*ENL(J)+ENL(J))*DELN(J)
      51      IF (SUM1.LT.0.) SUM1=-SUM1
      52      IF (SUM1.LT.AMDOA1) AMDOA1 = SUM1
      53      917  CONTINUE
      54      IF (SUM.GT.2.) AMBLA=2./SUM
      55      IF (AMBLA.LT.AMDOA) AMDOA = AMBLA
      56      IF (.NOT. IDEBUG) GO TO 111
      57      WRITE(6,923) IT,ENN,ENM,PP,PPLN,A
      58      923  FORMAT (3HIT,1E15.3,6H ENN,PP,PPLN,A
      59      1 7H PPLN=1E15.8,3H AMDOA=E15.8 )
      60      924  FORMAT(1X,2H0,1X,2H1,1X,2H2,1X,2H3,1X,2H4,1X,
      61      1R,.12X,6H-G0/RT,9X,5H-G/RT )
      62      DO 926 J=1,NS
      63      FNEG1 = S(J)-HO(J)
      64      FNEG2 = FNEG1

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SUBROUTINE EQLBM FORTRAN EXTENDED VERSION 2.0

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SUBROUTINE EQLBAM FORTRAN EXTENDED VERSION 2.0          31/12/770      08.09.56.
      FF=1.05*(J-1)*0.07-FNEG2=FNEG2-ERLN(M(J)-T)
      WRITE (6,325) SUB(J,1),SU9(J,2),
      1SUB(J,3),CN(J,NPT),ENLN(J),DELN(J),H3(J),S(J),FNEG1,FNEG2
      325 FORMAT (1X,3A4,7E15.6)
      326 CCNTINUE
      WRITE (6,110)
      110 FORMAT(1M0)
      220      C   APPLY CORRECTIONS TO ESTIMATES
      C
      111  SU4 = 0.
      00  113  J=1,NS
      112  ENLN(J)=ENLN(J)+AN30A*DELN(J)
      EN(J,NPT) = J.
      IF ((LEN(NJ)-ENNL+SIZE)*LE.0.) GO TO 113
      EN(J) = EXP(ENLN(J))
      SUM = SUM+EN(J,NPT)
      GO TO 113
      114  EN(J,NPT) = EN(J,NPT) + AN30A * DELN(J)
      115  CONTINUE
      113  SUMN = SU4
      IF (TP) GO TO 115
      TLN= TLN+AN30A*ULN
      T= EXP(T)
      115  ENNL = ENNL+AN30A*X(IG1)
      ENN = EXP(ENN)
      IF (LLMT(L).NE.IE) GO TO 116
      116  CONTINUE
      00  116  J = 1,NS
      IF (A(L,J)*EG(0,0) .GT. 0.) GC TO 1116
      IF (EN(J,NPT).GT.0.) GO TO 116
      1116  CONTINUE
      00  1116  J=1,NS
      IF (ATT(J),NE,0.) FUSE(J) = -10000
      1110  CONTINUE
      L = L-1
      IC1 = IG1-1
      GC TO 43
      240      C   CHECK ON REMOVING IONS
      C
      00  116  J = 1,NS
      IF (A(L,J)*EG(0,0) .GT. 0.) GC TO 1116
      IF (EN(J,NPT).GT.0.) GO TO 116
      1116  CONTINUE
      00  1116  J=1,NS
      IF (ATT(J),NE,0.) FUSE(J) = -10000
      1110  CONTINUE
      L = L-1
      IC1 = IG1-1
      GC TO 43
      250      C   TEST-FOR-CONVERGENCE
      C
      116  IF (ITNUM.B.EQ.0) GO TO 113
      IF (AMB0A.LT.1.) GO TO 43
      SUM = (ENN-SUM)/ENN
      IF (SUM.LT.0.) SUM = -SUM
      IF (SUM.GT.0.5E-5) GO TO 43
      00  130  J=1,NS
      IF (IUSE(J).LT.0) GO TO 130
      AA= DELN(J)/SUMN
      IF (AA.LT.0.) AA=-AA
      260

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## SUBROUTINE EOLGRM FORTRAN EXTENDED VERSION 2.0

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      IF (TUSE(J).EQ.0) NE= ALEN(J,NPT)          P1712 --> G16
129  IF(IAA.GT.J-.5.E-5) GO TO 45          P1712 0.91
130  CONTINUE                                P1712 0.920
13 CONV=.TRUE.
14 IF(1.1.LT.FLCON(.OR..11.GT.THGH.AND..10E3BUG) WRITE(6,336) IT,NPT
306  FORMAT(L10NTE TEMPERATURE=E12.4,26H IS OUT OF RANGE FOR PCINT,15) P1712 0.922
1471NUT,J) GO TO 165          P1712 0.923
1471NUT,J) IT,NPT          P1712 0.924
1473  FORMAT(1H,12.6SH ITERATIONS DID NOT SATISFY CONVERGENCE REQUIREME P1712 0.925
1475  IATS FOR THE POINT          P1712 0.926
1476  1IF 1.AOT.HP. OR.NPT.NE.1.DR.EQ.3.OR.IT.GT.67 IT.GT.67          P1712 0.927
1477  WRITE(6,474)          P1712 0.928
1477  IT=IT+1          P1712 0.929
1478  RETURN          P1712 0.930
1478
1479  C CONVERGENCE TESTS ARE SATISFIED, TEST CONDENSED SPECIES.          P1712 0.931
1480  C          P1712 0.932
1480  160  IF(INC.EC.G) GO TO 145          P1712 0.933
1480  SIZEF = 0          P1712 0.934
1480  INC = 0          P1712 0.935
1480  00 170 J = 1,NS          P1712 0.936
1480  IF (TUSE(J)).EQ.0 .OR. TUSE(J).EQ.-1000000 GO TO 170          P1712 0.937
1480  INC + 1          P1712 0.938
1480  IF (IDERUG) WRIT(6,146)(SUB(J,I),I=1,3),TEMP(INC,i),TEMP(INC,2),          P1712 0.939
1480  TUSE(J),NPT          P1712 0.940
1480
1481  144  FORMAT(1H0,3A4,2FI0.3,3X,5HUSE=,I4,C15.7)
1481  145  IF (EN(J,NPT)) 146,146,154          P1712 0.941
1481  146  IF (J.U.NF.JSOL .AND. J .NE. JL2) GO TO 147          P1712 0.942
1481  JSOL = 0          P1712 0.943
1481  JL1G = 0          P1712 0.944
1481  147  TGT = TGT - 1          P1712 0.945
1481  EN(J,NPT) = 0.          P1712 0.946
1481  GO TO 166          P1712 0.947
1481  :+9 KG = 1          P1712 0.948
1481  151  IF (TUSE(J)+ED-.4*USE(J+1)) GO TO 154          P1712 0.949
1481  151  IF (J.U.EC.1.0R.IUSE(J),NE,-IUSE(J-1)) GO TO 153          P1712 0.950
1481  KG = 1          P1712 0.951
1481
1482  154  JKG = J + KG          P1712 0.952
1482  IF (EN(J,KG,NPT).LT.C) GO TO 170          P1712 0.953
1482  TKELT = TEMP(INC,1)          P1712 0.954
1482  IMP = INC + KG          P1712 0.955
1482  IF (TKELT.EQ.1500) 150 TO 151          P1712 0.956
1482  :NEXT - TEMP(INC,2)
1482  IF (TKELT.EQ.1500) 151 TO 157          P1712 0.957
1482  WRITE(6,156)          P1712 0.958
1482  156  FORMAT(15OH3 PHASES OF A CONDENSED SPECIES ARE OUT OF ORDER )          P1712 0.959
1482
1483  C JTM SPECIES A SOLID (EN=0), (J>KG)TH SPECIES A LIQUID (EN IS +)          P1712 0.960
1483  C          P1712 0.961
1483  157  IF (IT.GT.TMELT) GO TO 169          P1712 0.962
1483  IF (T.P AND. IT.EQ.TMELT) GO TO 169          P1712 0.963
1483  IF (ITP) GO TO 1165          P1712 0.964
1483  IF (IT.LE.TMELT-150,) GO TO 1165          P1712 0.965
1483

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## SUBROUTINE EQBLRM FORTRAN EXTENDED VERSION 2.0

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330      J1Q = JK6
          GO TO 159
C   JTM SPECIES A LIQUID(EN=0), (J+KG)TH SPECIES A SOLID (EN IS +)
C
325      IF (TP.AND.TT.EQ.TMELT) GO TO 169
          IF (TP) GO TO 1165
          IF (TT.GE.TMELT+150.) GO TO 1165
          JSCL = JK6
          JLIU = J
          JLIU = -J
          TT = TMELT
          EN(JKG,NPT) = .5 * EN1JKG,NPT)
          EN(J,NPT) = EN(JKG,NPT)
          GC TC 165
C   WRONG PHASE--INCHEDO-FOR-T INTERVAL;--SWITCH TN
335      C
C   1165 EN(J,NPT) = EN (JK6, NPT)
          IUSE(J) = -IUSE(J)
          IUSE (JKG) = -IUSE (JKG)
          EN(JKG,NPT)= 0.
          EN(JKG,NPT)= 0.
          GO TO 160
          153 IF (TT.LT.TEMP(INC,1) * AND TEMP(INC,1) * NE.1LOW) GO TO 169
          IF (TT.GT.TEMP(INC,2)) GO TO 169
          C
          C
          SUM = 0.
          DO 167 T = T1C
              SUM = SUM + A(I,J)*X(I)
150      167 CONTINUE
          DELF = H1(J)-S1(J)-SUM
          IF (DELFG <=0) WRITE(6,168) DELF,SIZEF
          168 FORMAT (17H G0-SUM(AIJ*PI) =E15.7,10X,18H PREVIOUS DELTA S =,E15.7)
          359      169 IF (DE-F6E;SIZEF-NR.. DELF.GE.0.;.60-10 169
          SIZEF = DELF
          JOELF = J
          169 IF (ING.EQ.NC1) GO TO 143
          170 CONTINUE
          1165 IF (SIZEF.EQ.0.) GO TO 143
          1165 IF (.NOT.DELF)
              165 IC1 = IC1 + 1
              166 IUSE(J) = - IUSE(J)
              4n CONVG = .FALSE.
              143 TN = NUM3
              IF (10DEBUG) WRITE(6,771) NPT, (X(I),IL=1,L), TN
              771 FORMAT (1F3,14F9.3)
              ITAUM3 = 1TN
              GO TO 143
C   CALCULATE EQUILIBRIUM PROPERTIES
370      C

```

## SUBROUTINE E0-BRM FORTAN EXTENDED VERSION 2.0

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```

C 171 SSUM(NPT) = 0.
C     IF(JLT0.NE.0) EN(J$0L,NPT)=EN$0L
      DO 185 J=1,NS
      IF (NPT.EQ.1) SS0 = SS0 + EN(J,1)*S(J)
      SS = S(J)
      IF (IUSE(J,J).EQ.0) SS=SS-EN(J,NPT)-T4
      SSUM(NPT) = SSUM(NPT)+SS*EN(J,NPT)
      P1712 01024
      P1712 01025
      P1712 01026
      P1712 01027
      P1712 01028
      P1712 01029
      P1712 01030
      P1712 01031
      P1712 01032
      P1712 01033
      P1712 01034
      P1712 01035
      P1712 01036
      P1712 01037
      P1712 01038
      P1712 01039
      P1712 01040
      P1712 01041
      P1712 01042
      P1712 01043
      P1712 01044
      P1712 01045
      P1712 01046
      P1712 01047
      P1712 01048
      P1712 01049
      P1712 01050
      P1712 01051
      P1712 01052
      P1712 01053
      P1712 01054
      P1712 01055
      P1712 01056
      P1712 01057
      P1712 01058
      P1712 01059
      P1712 01060
      P1712 01061
      P1712 01062
      P1712 01063
      P1712 01064
      P1712 01065
      P1712 01066
      P1712 01067
      P1712 01068

C 175
      IF(JLT0.NE.0) EN(J$0L,NPT)=EN$0L
      DO 185 J=1,NS
      IF (NPT.EQ.1) SS0 = SS0 + EN(J,1)*S(J)
      SS = S(J)
      IF (IUSE(J,J).EQ.0) SS=SS-EN(J,NPT)-T4
      SSUM(NPT) = SSUM(NPT)+SS*EN(J,NPT)
      P1712 01024
      P1712 01025
      P1712 01026
      P1712 01027
      P1712 01028
      P1712 01029
      P1712 01030
      P1712 01031
      P1712 01032
      P1712 01033
      P1712 01034
      P1712 01035
      P1712 01036
      P1712 01037
      P1712 01038
      P1712 01039
      P1712 01040
      P1712 01041
      P1712 01042
      P1712 01043
      P1712 01044
      P1712 01045
      P1712 01046
      P1712 01047
      P1712 01048
      P1712 01049
      P1712 01050
      P1712 01051
      P1712 01052
      P1712 01053
      P1712 01054
      P1712 01055
      P1712 01056
      P1712 01057
      P1712 01058
      P1712 01059
      P1712 01060
      P1712 01061
      P1712 01062
      P1712 01063
      P1712 01064
      P1712 01065
      P1712 01066
      P1712 01067
      P1712 01068

C 183 CONTINUE
      IF (.NOT.IC) GO TO 176
      DLVPT(NPT) = -1.
      DLV1P(NPT) = 1.
      CP7TNPT) = CPSUM
      P1712 01024
      P1712 01025
      P1712 01026
      P1712 01027
      P1712 01028
      P1712 01029
      P1712 01030
      P1712 01031
      P1712 01032
      P1712 01033
      P1712 01034
      P1712 01035
      P1712 01036
      P1712 01037
      P1712 01038
      P1712 01039
      P1712 01040
      P1712 01041
      P1712 01042
      P1712 01043
      P1712 01044
      P1712 01045
      P1712 01046
      P1712 01047
      P1712 01048
      P1712 01049
      P1712 01050
      P1712 01051
      P1712 01052
      P1712 01053
      P1712 01054
      P1712 01055
      P1712 01056
      P1712 01057
      P1712 01058
      P1712 01059
      P1712 01060
      P1712 01061
      P1712 01062
      P1712 01063
      P1712 01064
      P1712 01065
      P1712 01066
      P1712 01067
      P1712 01068

C 185
      IF(JLT0.EQ.0) GO TO 199
      DC 179 J = 1,L
      SUM = SUM + PROK(J)*X(JJ)
      P1712 01024
      P1712 01025
      P1712 01026
      P1712 01027
      P1712 01028
      P1712 01029
      P1712 01030
      P1712 01031
      P1712 01032
      P1712 01033
      P1712 01034
      P1712 01035
      P1712 01036
      P1712 01037
      P1712 01038
      P1712 01039
      P1712 01040
      P1712 01041
      P1712 01042
      P1712 01043
      P1712 01044
      P1712 01045
      P1712 01046
      P1712 01047
      P1712 01048
      P1712 01049
      P1712 01050
      P1712 01051
      P1712 01052
      P1712 01053
      P1712 01054
      P1712 01055
      P1712 01056
      P1712 01057
      P1712 01058
      P1712 01059
      P1712 01060
      P1712 01061
      P1712 01062
      P1712 01063
      P1712 01064
      P1712 01065
      P1712 01066
      P1712 01067
      P1712 01068

C 199 GAMMAS(NPT) = -1./ (DLVPT(NPT) + (DLVTP(NPT)**2)*ENN/GPR(NPT))
      IUSE(JL1Q) = -IUSE(JL1Q)
      HSUM(NPT) = HSUM(NPT)+EN(JL1Q,NPT)*(H0(JL1Q)-H0(J$0L))
      P1712 01024
      P1712 01025
      P1712 01026
      P1712 01027
      P1712 01028
      P1712 01029
      P1712 01030
      P1712 01031
      P1712 01032
      P1712 01033
      P1712 01034
      P1712 01035
      P1712 01036
      P1712 01037
      P1712 01038
      P1712 01039
      P1712 01040
      P1712 01041
      P1712 01042
      P1712 01043
      P1712 01044
      P1712 01045
      P1712 01046
      P1712 01047
      P1712 01048
      P1712 01049
      P1712 01050
      P1712 01051
      P1712 01052
      P1712 01053
      P1712 01054
      P1712 01055
      P1712 01056
      P1712 01057
      P1712 01058
      P1712 01059
      P1712 01060
      P1712 01061
      P1712 01062
      P1712 01063
      P1712 01064
      P1712 01065
      P1712 01066
      P1712 01067
      P1712 01068

C 200 IF (.NOT.I$EBUG) RETURN
      WRITE(6,201) NPT,PCP(NPT),PP,TT,HSUM(NPT),WM(NPT),GPR(NP)
      P1712 01024
      P1712 01025
      P1712 01026
      P1712 01027
      P1712 01028
      P1712 01029
      P1712 01030
      P1712 01031
      P1712 01032
      P1712 01033
      P1712 01034
      P1712 01035
      P1712 01036
      P1712 01037
      P1712 01038
      P1712 01039
      P1712 01040
      P1712 01041
      P1712 01042
      P1712 01043
      P1712 01044
      P1712 01045
      P1712 01046
      P1712 01047
      P1712 01048
      P1712 01049
      P1712 01050
      P1712 01051
      P1712 01052
      P1712 01053
      P1712 01054
      P1712 01055
      P1712 01056
      P1712 01057
      P1712 01058
      P1712 01059
      P1712 01060
      P1712 01061
      P1712 01062
      P1712 01063
      P1712 01064
      P1712 01065
      P1712 01066
      P1712 01067
      P1712 01068

C 205
      FORMT(7MPOINT)=13,3X+4MPC=E13.6,3X,2HP=E13.6*3X,2HT=E13.6*3X,4H
      1H/R=E13.6,3X,4HS/R=E13.6/3X,3HMM=E13.6,3X,5HCP/R=E13.6,3X,6HD,VPT
      2-E13.6,3X,3HDT,VPT=E13.6,3X,5HCPMMAS(S)=E13.6
      P1712 01024
      P1712 01025
      P1712 01026
      P1712 01027
      P1712 01028
      P1712 01029
      P1712 01030
      P1712 01031
      P1712 01032
      P1712 01033
      P1712 01034
      P1712 01035
      P1712 01036
      P1712 01037
      P1712 01038
      P1712 01039
      P1712 01040
      P1712 01041
      P1712 01042
      P1712 01043
      P1712 01044
      P1712 01045
      P1712 01046
      P1712 01047
      P1712 01048
      P1712 01049
      P1712 01050
      P1712 01051
      P1712 01052
      P1712 01053
      P1712 01054
      P1712 01055
      P1712 01056
      P1712 01057
      P1712 01058
      P1712 01059
      P1712 01060
      P1712 01061
      P1712 01062
      P1712 01063
      P1712 01064
      P1712 01065
      P1712 01066
      P1712 01067
      P1712 01068

C 210
      C   ERROR, SET TT=0
      C
      C 873 TT=0.
      C
      C 1000 RETURN
      C
      C 415
      NPT = NPT-1
      1000
      EN
      P1712 01024
      P1712 01025
      P1712 01026
      P1712 01027
      P1712 01028
      P1712 01029
      P1712 01030
      P1712 01031
      P1712 01032
      P1712 01033
      P1712 01034
      P1712 01035
      P1712 01036
      P1712 01037
      P1712 01038
      P1712 01039
      P1712 01040
      P1712 01041
      P1712 01042
      P1712 01043
      P1712 01044
      P1712 01045
      P1712 01046
      P1712 01047
      P1712 01048
      P1712 01049
      P1712 01050
      P1712 01051
      P1712 01052
      P1712 01053
      P1712 01054
      P1712 01055
      P1712 01056
      P1712 01057
      P1712 01058
      P1712 01059
      P1712 01060
      P1712 01061
      P1712 01062
      P1712 01063
      P1712 01064
      P1712 01065
      P1712 01066
      P1712 01067
      P1712 01068

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      55      CONTINUE
      IF (CONVG) GO TO 81
      ULNT = (SUMS-SOY)/CPSUM
      TLN = TLN-ULNT
      IF (DLNT .LT. 0.) DLNT = -DLNT
      IF (DLNT .LT. 0.5E-4) CONVG = .TRUE.
      GO TO 51
      60      ITI(NPT) = ITI
      SSUM(NPT) = SSUM(1)
      HSUM(NPT) = ITI*SUMH
      GAMMAS(NPT) = CPSUM/(CPSUM-HSUM(1)/WM(1))
      IF (IP .GT. 2) GO TO 90
      C
      C   THROAT CALCULATIONS
      C
      OH = HSUM(1)-HSUM(2)
      DNSTAR = OH-(GAMMAS(2)*ITI/(12.*WM(1)))
      DH = DNSTAR/DH
      ITI=ITI-DNSTAR/DH
      ITI=ITI-DNSTAR/DH
      IF (OH .LE. 0.4E-4 .OR. ITROT.EQ.0.) GO TO 90
      PCP(2) = PCP(2)/11.+2.*DH*STAR*WM(1)/(IT*(GAMMAS(2)+1.1))
      P(2) = P(1)/PCP(2)
      ITROT = ITROT-1
      GO TO 45
      70      ITI=ITI-NPT/2-NPT
      PNP(NPT) = P(IP)
      CPNP(NPT) = CPSUM
      K = 0
      IF (IT.LT.(ITLOW-150.)) GO TO 903
      IF (INC .EQ. 0.) GO TO 700
      INC = 0
      80      801  I=1,NS
      IF (IUSE(1).EQ.0 .OR. IUSE(1).EQ.-100000) GO TO 901
      INC = INC+1
      IF (EM(1,1).EQ.0.) GO TO 901
      IF (IT.LT.(TEMP(INC,1)-50.) .OR. IT.GT.(TEMP(:,:,-2)+50.)) GO TO 903
      IF (INC .EQ. 0.) GO TO 700
      85      852  CONTINUE
      700  IF (IP.EQ.NP) GO TO 863
      K = MPT
      IF (NPT.NE.13) GO TO 870
      GO TO 863
      95      903  NP1 = NPT - 1
      863  GHT = RKT007
      IF (NSUB+NSUP.NE.0) CALL RATIO
      865  IF (K.EQ.0) GO TO 1003
      NPT = 2
      870  NPT = NPT + 1
      902  CONTINUE
      1000  RETURN
      END
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      P1712  01122
      P1712  01123
      P1712  01124
      P1712  01125
      P1712  01126
      P1712  01127
      P1712  01128
      P1712  01129
      P1712  01130
      P1712  01131
      P1712  01132
      P1712  01133
      P1712  01134
      P1712  01135
      P1712  01136
      P1712  01137
      P1712  01138
      P1712  01139
      P1712  01140
      P1712  01141
      P1712  01142
      P1712  01143
      P1712  01144
      P1712  01145
      P1712  01146
      P1712  01147
      P1712  01148
      P1712  01149
      P1712  01150
      P1712  01151
      P1712  01152
      P1712  01153
      P1712  01154
      P1712  01155
      P1712  01156
      P1712  01157
      P1712  01158
      P1712  01159
      P1712  01160
      P1712  01161
      P1712  01162
      P1712  01163
      P1712  01164
      P1712  01165
      P1712  01166
      P1712  01167
      P1712  01168
      P1712  01169
      P1712  01170
      P1712  01171

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C          SUBROUTINE MCALC
C          CALCULATE ENTHALPY FOR PROPELLANT USING COEFFICIENTS
05      C          LOGICAL MOLES
               DIMENTION-NUM15-5,MS121
               P1712 01172
               P1712 01173
               P1712 01174
               P1712 01175
               P1712 01176
               P1712 01177
               P1712 01178
               P1712 01179
               P1712 01180
               P1712 01181
               P1712 01182
               P1712 01183
               P1712 01184
               P1712 01185
               P1712 01186
               P1712 01187
               P1712 01188
               P1712 01189
               P1712 01190
               P1712 01191
               P1712 01192
               P1712 01193
               P1712 01194
               P1712 01195
               P1712 01196
               P1712 01197
               P1712 01198
               P1712 01199
               P1712 01200
               P1712 01201
               P1712 01202
               P1712 01203
               P1712 01204
               P1712 01205
               P1712 01206
               P1712 01207
               P1712 01208
               P1712 01209
               P1712 01210
               P1712 01211
               P1712 01212
               P1712 01213
               P1712 01214
               P1712 01215
               P1712 01216
               P1712 01217
               P1712 01218
               P1712 01219
               P1712 01220
               P1712 01221
               P1712 01222
               P1712 01223
               P1712 01224

10      C          COMMON/SPECES/CODEF(2,7,150),S(150),EN(150,13),ENLN(150),M(150)
               1,DELR(150),A(15,50),SUB(150,31),IUSE(150),TEMP(50,2)
               GOMMON/MISC/ENV,SUMN,T,T0,ATOM(4,101),LLMT(151,30(15),80P(15,2)
               1,TH,TLCH,THIGH,P,CPSUM,OF,EORAT,FPCT,R,RR,HSUB0,AC(2),AM(2)
               2,VMPT(2),RHDT(2),THMT(2),WPL-S12),MP(2),DATA(227,NAME15,V
               3,ANUM(15,5),PECM(15),ENTH(15),FAZ(15),FOX(15),DENS(15)
               4,RHOP,RMW(15),TLN,JANF
               COMMON/INOKX/IDEBUG,CONVG,TP,HPS,SP,HPSV,MOLES,NP,NT,NPT,L,NS,
               1,KMAT,IMAT,IDA,N,J,NOMIT,IP,NEAR,NSUP,IT,NGPCVFRC,PVCVEQ
               2,TONS,NC,INSERT,JSL,JIJQ,KASE(14),NRREAC,IC,IQZ
               EQUivalence(LANUP,NUM)
               DATA AG/1HG/,*IZERO/2H00/*,0X/1H0/
               C          IS IT IN RANGE
25      C          IF(IT,LT,(TLOW-100.),OR,IT,GT,(THIGH+1000.))GO TO 80
               MS(1) = 0.
               MS(2) = 0.
               HPP(1) = 0.
               HPP(2) = 0.
               K=2
               IF(FOX(N).EQ.0)K=1
               PCMT=PECMT(N)
               IF(THOT-E)PCMT=PCMT+RMH(N)
               HS(K) = HS(K) + PCMT
               J = NUM(N,5)
               IF ((J,NE,3) UC 10 30
               DO 11 J=1,L
               DATA(J)=0.
               1P-CONTINUE
               00 40 I=1,4
               IF (IANUM(N,I).EQ.0) GO TO 53
               00 20 J=1,L
               IF (LLMT(I).EQ.NAME(N,I)) GO TO 30
               20 CONTINUE
               30 DATA(J)=ANUM(N,I)
               53 5R 1S=0
               40 CONTINUE
               00 70 J=1,NS
               IF(IUSE(J).EQ.0)GO TO 55

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## SUBROUTINE MCALC FORTRAN EXTENDED VERSION 2.0

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IS = 1547
IF (FAZ(N) .EQ. AG) GO TO 70
IF ITT.LY.TEMP (IS,1).OR.ITT.JT.TEMP (IS,2)) GO TO 70
GO TO 56
56 IF (FAZ(N) .NE. AG) GO TO 70
IF (FAZ(N) .EQ. AG) GO TO 10
DO 60 I=1,L
IF (TT(J),JT,JONE,DATATT) GO TO 70
60 CONTINUE
NU4(N,5) = J
GO TO 90
70 CONTINUE
GO TO 60
90 NSS = HE
NS = J
CALL CPS
CPSUM = CPSUM/EN(J,NPT)
NS = NSS
IF (HO(J) .GT. -.01 .AND. HO(J) .LT. .01) HO(J) = 0.
RTEMPNT = RTT
ENTH(N) = MU(J)*RTT
AC(K) = AC(K)+CPUM*PCM/RCMN(N)
HPP(K) = HPP(K)+PCM/RCMN(N)
CONTINUE
950 DO 950 K=1,2
IF (TPTKT*ET(J).GT.0.95) --
HPP(K) = HPP(K)/MS(K)
AC(K) = AC(K)/MS(K)
CONTINUE
950
HS00J = (WP(1)*HPP(1)+WP(2)*HPP(2))/(WP(1)+WP(2))
DO 1000 GO TO 1000
1000 WRITE(J,95) N
95 FORMAT (1H0,12.34HITH REACTANT IS NOT IN THERMO DATA )
1100 RETURN
END

```

P1712 01225

P1712 01226

P1712 01227

P1712 01228

P1712 01229

P1712 01230

P1712 01231

P1712 01232

P1712 01233

P1712 01234

P1712 01235

P1712 01236

P1712 01237

P1712 01238

P1712 01239

P1712 01240

P1712 01241

P1712 01242

P1712 01243

P1712 01244

P1712 01245

P1712 01246

P1712 01247

P1712 01248

P1712 01249

P1712 01250

P1712 01251

P1712 01252

P1712 01253

P1712 01254

P1712 01255

P1712 01256

P1712 01257

P1712 01258

## SUBROUTINE MATRIX FORTRAN EXTENDED VERSION 2.0

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      C   SUBROUTINE MATRIX
      C
      C   DOUBLE PRECISION G,X
      C   LOGICAL HP,SP,TF,IDEBUG,CONVG,NEWR
      C
      05    C   COMMON/POINTS/HSUM(13),SSUM(13),CPR(13),DVTP(13),UVEPT(13)
      C   1  *GAM48(13),P(26),T(26),V(13),PP(13),WM(13),SONVEL(13),TT(13)
      C   2  .TCTN(13),EN(150),S(150),ENL(150),MD(150)
      C   COMMON/SPECES/COEF(2,7,150),S(150),EN(150),1USE(150),TEMP(50,2)
      C   1 ,DELN(15),A(15,150),S(150,150),SU(150,3),IUSE(150),LLMT(15),BOP(15,2)
      C   COMMON/MSC/ENN,SUMN,TI,SU,ATOM(3,114),LLMT(15),BOP(15,2)
      C
      C   T,TR,TLCAT,THIGH,PF,TCRUM,OF,FORQ,FRCT,R,PRT,HSURB,AUT27,ANT27,P1712,U1265
      C   2  *MP(2)*RHO(2),VMIN(2,VMLS(2),MP(2),NAME(15,5),
      C   3 ,ANUM(15,7),PECHT(15),ENTH(15),FAZ(15),RTMP(15),FOX(15),DENS(15)
      C   4 ,RHOP,RW(15),ILN,JANF
      C   COMMON/DDOUBLE/ G(620,21),X(20)
      C   COMMON/INDEX/ IDEBUG,CONVG,TP,HP,SP,HPSP,TPSP,MOLES,NP,NT,HPT,L,NS, P1712,U1266
      C   1  *NMAT,ITAT,IT1,NM1,NOMIT,IP,NEWR,NSUB,NSUP,TIN,CPUVFR,CPGVED P1712,U1267
      C   2 ,IONS,AC,NSERT,JSCL,JLIO,KASE(14),NREAC,IC,IC2
      C
      20    C   IO2 = IO1 + 1
      C   IO3 = IO2 + 1
      C   KMAT = IO3
      C   IFY,ROT,CONVG,AND,TP1 KMAT = IO2
      C   IMAT = KMAT - 1
      C
      25    C   CLEAR MATRIX STORAGE TO ZERO
      C
      30    C   DO 211 L=1,IMAT
      C   DO 211 K1,KMAT
      C   G(I,K) = 0.000
      C   G(I,K1) = 0.0
      C
      63    C   211 CONTINUE
      C   SSS = 0.
      C   HSUM(NFT) = 0.
      C
      35    C   BEGIN SET UP OF ITERATION MATRIX
      C
      40    C   KK = L
      C   DO 65 J=1,NS
      C   H=MU(J)*EN(J,NPT)
      C
      45    C   IF -(TOSCF(J))-.85,I2,.70
      C   19 F = (H(1,J))-S(1,J)+ENLN(J)+TM)*EN(J,NPT)
      C   TERM1 = H
      C   IF (KMAT .EQ. IC2) TERM1 = F
      C   DO 55 I = 1, L
      C
      50    C   CALCULATE THE ELEMENTS R(I,K)
      C
      45    C   IF (A(I,J) .EQ. 0.) GO TO 55
      C   TERM= A(I,J)*EN(J,NPT)
      C
      50    C   P1712,U1268
      C   P1712,U1269
      C   P1712,U1270
      C   P1712,U1271
      C   P1712,U1272
      C   P1712,U1273
      C   P1712,U1274
      C   P1712,U1275
      C   P1712,U1276
      C   P1712,U1277
      C   P1712,U1278
      C   P1712,U1279
      C   P1712,U1280
      C   P1712,U1281
      C   P1712,U1282
      C   P1712,U1283
      C   P1712,U1284
      C   P1712,U1285
      C   P1712,U1286
      C   P1712,U1287
      C   P1712,U1288
      C   P1712,U1289
      C   P1712,U1290
      C   P1712,U1291
      C   P1712,U1292
      C   P1712,U1293
      C   P1712,U1294
      C   P1712,U1295
      C   P1712,U1296
      C   P1712,U1297
      C   P1712,U1298
      C   P1712,U1299
      C   P1712,U1300
      C   P1712,U1301
      C   P1712,U1302
      C   P1712,U1303
      C   P1712,U1304
      C   P1712,U1305
      C   P1712,U1306
      C   P1712,U1307
      C   P1712,U1308
      C   P1712,U1309
      C   P1712,U1310
      C   P1712,U1311
  
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## SUBROUTINE MATRIX FORTRAN EXTENDED VERSION 2.0

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55      DC 19  PRINT
      G(I,K)=G(I,K)+A(I,J)*TER2
      15  CONTINUE
      C
      G(I,I01)=G(I,I01)+TERM1
      G(I,I02)=G(I,I02)+A(I,J)*TERM1
      IF (ISP) G(I,I02)=G(I,I02)+A(I,J)*F
      55  CONTINUE
      IF (KMAT .EQ. 1) = G(I,I02)+A(I,J)*SS
      IF (CONVG,02,HP) GO TO 59
      65      GTRUE,FTEST=0.02,100,100,100
      G(I02,I02)=G(I02,I02)+M0(J,J)*SS
      G(I02,I03)=G(I02,I03)+(S(JJ)-ENLN(JJ)-TM)*F
      GO TO 62
      59  G(I02,I02)=G(I02,I02)+M0(J,J)*H
      IF (CONVG) GO TO 64
      GTRUE,FTEST=0.02,100,100,100
      62  G(I01,I03)=G(I01,I03)+F
      64  G(I01,I02)=G(I01,I02)+TERM
      70
      75      C
      C CONDENSED SPECIES
      C
      79  KK = KK + 1
      80  DO 75  J = I,L
      G(I,KK) = A(I,J)
      G(I,KMAT) = G(I,KMAT) - A(I,J)*EN(J,NPT)
      75  CONTINUE
      C
      G(IKK,KMAT) = H0(JJ) - S(J)
      HSUM(NPT) = HSUM(NPT) + H
      IF (.NOT.ISP) GO TO 55
      G(IQ1,IQ1) = SUPN - ENN
      SSS = S(J) * EN(J,NPT)
      G(I02,KK) = S(J)
      85      SSS = SSS + G(I02,I01)
      HSUM(NPT) = HSUM(NPT) + G(I01,I02)
      G(IQ1,IQ1) = SUPN - ENN
      90
      95      C
      C REFLECT SYMMETRIC PORTIONS OF THE MATRIX
      C
      ISYM = I01
      IF (HP.OR.CONVG,ISYM=IC2
      00 102 1=1,ISYM
      00 102 1=1,ISYM
      GJ,I,J=G(I,J)
      100      102  CONTINUE
      105      C
      C COMPLETE THE RIGHT HAND SIDE
      C
      IF (CONVG) GO TO 175

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## SUBROUTINE MATRIX FORTRAN EXTENDED VERSION 2.0

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DC 145 I=1,L
X(1)=B(1)-G(1,IQ1)
G(1,KMAT) = G(1,KMAT)+X(1)
145 CONTINUE
G(IQ1,KMAT) = G(IQ1,KMAT)+ENN-SUMN
C
C COMPLETE ENERGY ROW AND TEMPERATURE COLUMN
C
115   IF (KMAT .EQ. IC2) GO TO 185
      IF (SP) ENERGY = S0+ENN-SUMN - SSS
      IF (HP) ENERGY=HSUROTT - HSUM(NPT)
      G(102,IC3)=G(102,103)+ENERGY
175   G(102,IC2)=G(IC2,102)+GPSUM
185   RETURN
      ENC
120

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## SUBROUTINE MGAUSC FORTNAN EXTENDED VERSION 2.0

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0d.09.56.

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      C SUBROUTINE MGAUSC
      C SOLVE ANY LINEAR SET OF UP TO 20 EQUATIONS
      C DOUBLE PRECISION G,X,COEFX(20),SUM,2
      C DIMENSION COEFX(20)
      C COMMON/COULE/G(20,21),X(20)
      C COMMON/INDA/ 10EBUG,CONVG,TP,HP,SP,MPSR,TSPS,MOLES,NP,NT,NPL,L,NS,
      1   RMAT,IMAT,101,N,J,HOMIT,IP,NEMR,NSUB,NSUP,I1N,CPCVFR,CFCVLO
      2   ,IONS,AC,INSERT,JSL,JILO,KASE(14),NP,EAC,IC,IC02
      C EQUIVALENCE I1USE,TIMATT
      15   C DATA BIGNO/1.E+38/
      C BEGIN ELIMINATION OF NINTH VARIABLE
      C I1USE=I1USE+1
      20   6 DO 45 NN=1,IUSE
           IF (NN-IUSE) 8,83,3
      83   IF (I1NN>NN) 31,23,31
      C SEARCH FOR MAXIMUM COEFFICIENT IN EACH ROW
      25   C 4 00 18 I>NN,IUSE
           COEFX(I) = BIGNO
           IF (I1,I,NN).EQ.0.) 60 TO 19
           COEFX(I) = 0.
           DO 10 J>NN,IUSE1
           SUM = GT(I,J)
           IF (SUM.LT.0.) SUM=-SUM
           IF (I1J>NN,NN) GO TO 9
           Z = SUM
           30   GC TO 10
           10 CONTINUE
           9 IF (SUM.GT.COEFX(I)) COEFX(I)=SUM
           10 CONTINUE
           COEFX(I) = COEFX(I)/Z
           18 CONTINUE
           TEMP = BIGNO
           I=0
           20   DO 22 J>NN,IUSE
           22 CONTINUE
           87 TEMP=COEFX(J)
           I=J
           15   22 CONTINUE
           IF (I) 28,23,28
           C INDEX I LOCATES EQUATION TO BE USED FOR ELIMINATING THE NTH
           50   C VARIABLE FROM THE REMAINING EQUATIONS
           C INTERCHANGE EQUATIONS I AND NN
           C
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      P1712 01432

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## SUBROUTINE 4GAUSO FORTRAN EXTENDED VERSION 2.0

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      28 IF(IWM-I) 29,31,29
      29 30 JANN,IUSE1
      30 Z=G(I,J)
      G(I,J)=G(NN,J)
      G(NN,J)=Z
      30 CONTINUE
      60          C
      C DIVIDE ARR ROW BY NTH DIAGONAL ELEMENT AND ELIMINATE THE NTH
      C VARIABLE FROM THE REMAINING EQUATIONS
      C
      31 K = NN + 1
      32 DO 36 J = K, IUSE1
      33   IF(G(NN,NN).EQ.0.) GO TO 23
      34   G(NN,J) = G(NN,J) / G(NN,NN)
      35 CONTINUE
      36 IF(K-IUSE1) 36,45,38
      37 38 DO 44 I = K,IUSE
      39   G(I,J) = G(I,J) - G(I,NN)*G(NN,J)
      40 DO 44 J = <, IUSE1
      41   G(I,J) = G(I,J) - G(I,NN)*G(NN,J)
      42 44 CONTINUE
      43 45 CONTINUE
      78          C
      C BACKSOLVE FOR THE VARIABLES
      C
      47 J = K + 1
      48 X(IK) = 0.000
      49 X(IK) = C(J,J)
      50 SUM = 0.0
      51 IF(IUSE - J) 51,49,58
      52 53 DO 56 I=1-3, IUSE
      53   SUM = SUM + G(X,I)* X(I)
      54 56 CONTINUE
      55   51 X(IK) = G(K,IUSE1) - SUM
      56   K = K - 1
      57   IF (K) 67,151,57
      58   58 -23- IUSE-2
      151 RETURN
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SUBROUTINE WOLTOP FORTRAN EXTENDED VERSION 2.0  
.....ENII,NFTI = ENII,K)  
55 680 CONTINUE  
902 GOATINUE  
1000 RETURN  
END

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- P1712 01525  
- P1712 01526  
- P1712 01527  
P1712 01527  
P1712 01526  
P1712 01529



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SUBROUTINE OUT1      FORTRAN EXTENDED VERSION 2.0          31/12/70      06.09.56.
-----+-----+-----+-----+-----+-----+-----+-----+-----+
      H01 = CX10
  55      H02 = ANT
           GO TO 11
  10      H01 = FUEL
           H02 = FB
  11      DO 13 J=1,5
           IF(TAUH(N,J),J=6:0,0) GO TO 14
  13      CONTINUE
           J=5
  14      J=J-1
           HEAD(3)=YN(J)
           HEAD(7)=YX(J)
           WRITE(SNAMEA) H01,H02,NAME(N,J,0),ANUM(N,J,0),J=1:6,PECM(N),ENTHT P1712 01582
           IND,FAZ(N),RTEMP(N),DENS(N)
  15      CONTINUE
           WRITE(6,20) OF,FPCT,EGRAT,RHOP
  20      FORMAT(1H0,15X,4H0/F=,F8.4,4X,13MPERCENT FUEL=,F8.4,4X,
           1 19HECUTVALENCE RATIO=,F7.4,4X,8HDENSITY=,F8.4/5
           C
           AGV = 9.80665
           DO 25 I = 1,NPT
           TOTN(I) = 0
           DO 25 J = 1,MS
           TOTN(I) = TOTN(I) + ENT(J,I)
  25      CONTINUE
           FMT(4)= FMT(6)
           RETURN
  60      C      ENTRY OUT2
  75      C      PRESSURE
  85      C      00 55 I=1,NPT
           K= 2*I+3
           FMT(K)= F4
           IF (PPP(I).GE.1.) FMT(K)=F3
           IF (PPP(I).GE.100.) FMT(K)=F2
           IF (PPP(I).GE.1000.) FMT(K)=F1
  90      SS      CONTINUE
           WRITE(6,FMT) (PP(I),I=1,L),(POP(J),J=1,NPT)
  95      C      TEMPERATURE
           00 65 I=1,NPT
           NV(I)= ITT(I)+.5
  100     65      CONTINUE
           FMT(6)= FMT13
           FMT(5)= FMT19
           WRITE(6,FMT) (F(I),I=1,L),(NV(J),J=1,NPT)
           C      FNTHALPY
  105     C      00 75 I=1,NPT

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           P1712 01634

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SUBROUTINE OUT: FORTRAN EXTENDED VERSION 2.0

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      VTT = HSUM(I)*R
      75  CONTINUE
      FMT(5) = FB
      FMT(7) = F1
      WRITE (6,FMT) (FH(I),I=1,4), (V(J),J=1,NPT)
      C
      C   ENTROPY
      C
      C   FMT(7)=F4
      DO 73 I = 1,NPT
      V(I) = SSUM(I) * R
      73  CONTINUE
      WRITE (6,FMT) (FS(I),I=1,4), (V(J),J=1,NPT)
      80  FORMAT (1H )
      C
      C   MOLECULAR WEIGHT
      C
      C   FMT(7)=F3
      WRITE (6,FMT) (FM(I),I=1,4), (WM(J),J=1,NPT)
      C
      C   QLV/DLPT
      C
      C   FMT(7)=F5
      IF(EQL) WRITE(6,FMT) (FV(I),I=1,4), (QVPT(J),J=1,NPT)
      125
      C
      C   QLV/DLT/P
      C
      C   FMT(7)=F5
      IF(EQL) WRITE(6,FMT) (FO(I),I=1,4), (QLVTP(J),J=1,NPT)
      130
      C
      C   HEAT CAPACITY
      C
      C   DO 85 I=1,NPT
      V(I) = CP(I) * R
      85  CONTINUE
      WRITE(6,FMT) (PCIT(I),I=1,NPT)
      135
      C
      C   GAMMAS
      C
      C   WRITE(6,FMT) ((GAMMAS(J),J=1,NPT)
      140
      C
      C   SONIC VELOCITY
      C
      C   145
      C
      C   FMT(7)= F1
      DO 95 I = 1,NPT
      SORVEL(I) = SQRT((R2*GAMMAS(I))*TTT(I)/WM(I))
      95  CONTINUE
      WRITE(6,FMT) (PCIT(I),I=1,NPT), (SORVEL(J),J=1,NPT)
      150
      C
      C   VOLUMC=GAMMAS(1)*TTT(1)
      VOLUMC=VOLUMC*2701./WM(1)
      IMPETUS=VOLUMC*2701./WM(1)
      RETURN
      C

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## SUBROUTINE OUT1 FORTAN EXTENDED VERSION 2.0

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08.09.56.

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160      ENTRY OUT1
        IF (.NOT.EOL) GO TO 331
        C      MOLE FRACTIONS - EQUILIBRIUM
        C      WRITE (6,80)
        80     FORMAT(6,310)
        310    FORMAT(15H MOLE FRACTIONS //)
          0N   330 K=1,NS
          DO   315 I=1,NPT
          V(I) = EN(K,I) / TOTN(I)
          315 CONTINUE
          0G   316 I=1,NPT
          IF (V(I).GE.(5.E-6)) GO TO 321
          316 CONTINUE
          GC TC 330
          320 WRITE (6,FMT) SUB(K,1),SUB(K,2),SUB(K,3),FB,(V(I),I=1,NPT)
          321 CONTINUE
          331 WRITE(6,335)
          335 FORMAT(11H ADDITIONAL PRODUCTS WHICH WERE CONSIDERED BUT WHOSE MO
          1LE FRACTIONS WERE LESS THAN .000005 FOR ALL ASSIGNED CONDITIONS//)
          LINE= 0
          0O   350 K=1,NS
          0- 340 I=1,NPT
          180    IF ((EN(K,I)/TOTN(I)).GE.(5.E-6)) GO TO 343
          343  CONTINUE
          73     LINE= LINE+1
          Z(LINE,1)= SUB(K,1)
          Z(LINE,2)= SUB(K,2)
          24-TIME=3)=SUBTK,3)
          190    343 IF ((LINE.NE.10) .AND. K.NE.NS) GO TO 350
          IF ((LINE.E2,6) GO TO 1000
          WRITE(6,345) (Z(LN,1),Z(LN,2),Z(LN,3),LN=1,LINE)
          345 FORMAT (10(1X,3A4))
          LINE= 0
          195    350 CONTINUE
          IF (.NOT.MOLE) WRITE(6,360)
          360 FORMAT(78HNOTE. WEIGHT FRACTION OF FUEL IN TOTAL FUELS AND OF OXI
          2DANT IN TOTAL OXIDANTS )
          200    WRITE(6,100) PMOLE
          1100   FORMAT(1H0 *VISCOISITY AND CONDUCTIVITY VALUES BASED ON *F5.1,* PE P171201 00003
          *CENT-OF-GAS-MIXTURE*)
          1000   RETURN
          ENC

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## SUBROUTINE RATIO FORTRAN EXTENDED VERSION 2.0

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      SUBROUTINE RATIO FORTRAN EXTENDED VERSION 2.0          31/12/70          08.19.56.
      C
      C     USED FOR AREA RATIO INTERPOLATION ONLY
      C
      05      C     DOUBLE PRECISION G,X
              C     LOGICAL EQL, FROZ,TPSP
      C
      C     DIMENSION PER(2,2),AI(13),APCP(13),AT(13),ANMT(13),RPP(2),NV(13)    P1712      01730
      1      C     RPP(2)
      C
      C     COMMON/POINTS/MSUM(13),SSUM(13),CPR(13),OLVTP(13),OLVPT(13),NM    P1712      01731
      1      ,GAMMAS(13),P(26),T(26),V(13),PPP(13),WM(13),SGNVEL(13),TT(13)    P1712      01732
      C
      15      COMMON/SPECIES/COEF(2,7,150),S(150),EN(150,13),ENLN(150),HQ(150)    P1712      01733
      1      ,JELN(150),A(15,150),SUB(150,3),IUSE(150),TEMP(50,2)    P1712      01734
      C
      1      COMMON/TISC/ENN,SUMN,TT,SD,ATOM(3,101),LLMT(15),BU(15),BOP(15,2)    P1712      01735
      1      ,TM,TION,TM10,THIGH,PP,CPSUM,OF,EQRAT,FPCT,R,RR,MSUB,AC(2),AM(2)    P1712      01736
      2      ,HPP(12),RHO(2),VMIN(2),VPLS(2),WP(2),DATA(22),NAME(15,5)    P1712      01737
      3      ,ANGHT(3,3),PCMT(3,3),FENTH(3),FAZ(2,3),RTEMP(15);FOXTISY,DENS(13)    P1712      01738
      4      RHOP,KMK(15),TLN,JANF
      C
      20      COMMON /DOUBLE/ E(120,23),X(20)
      C
      COMMON/INDEX/IOLBUG,CONVO,IP,HP,SP,HPSR,TPSP,MOLES,NP,NT,NPI,L,NS,    P1712      01739
      1      NMAT,IAIT,I01,N,J,NOMIT,IP,NEMR,NSUB,NSUP,ITN,CPCIFR,CPCVEJ
      2      IONS,AC,HSERT,JSOL,JLIO,CASE(14),READ,IC,IG2
      3      COMMON/NRNP/CP-(2857,YNMOT37,SPIMT37,ACI(13),SUBAR137,SUPAKT37,P1712      01740
      1      ,CPRF(13),AE(13),CSTR,EqL,FROZ,SSN
      74      COMMON/OUTP/FT(3,Y),FP(4),FT(4),FS(4),FM(4),FV(4),FU(4)    P1712      01741
      1      ,FC(4),FG(4),FB,FMT(3,F1,F2,F3,F4,F5,FL(4),F4T19,FA1,FA2
      2      ,FR1,FC1,FN(4),F2(4),FA(4),FI(4),F119X,F0
      30      C
      C     CONTINUENCE--VV,VV
      C
      40      NBLO = NPT-2
              DU 22 J=3,NPT
              IF (PCP(LJ).GT.PCP(2)) GO TO 30
      35      22
              CONTINUE
              GO TO -32
      30      NGLD-J-3
              31      DO 1200 ISONIC=1,2
              LL = 1
              IF (ISONIC.EQ.2) GO TO 34
              IF (NSUB.EQ.0) GO TO 1200
              NAR = NSUB
              GO TO 36
      45      34      IF (NSUP.EQ.0) GO TO 1200
              NAR = NSUP
              36      DO 1100 I=1,NAR
              IF (ISONIC.EQ.2) GO TO 40
              IF (ISONIC.EQ.0) GO TO -1468
              FF=FNR-D-E-11-GO TO 40
              K=2+NBL0
              DO 36 J=4,K
              J=JJ
              V(IJJ) = SUBAR(I)
      50
      
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SUBROUTINE RATIO FORTRAN EXTENDED VERSION 2.0          31/12/70
      IF(V(LLL),GE,KEAT(JJ)) GO TO 56
      56   38 CONTINUE
           GO TO 56
      40   IF(NPNT-NBL>LE-3) GO TO 1100
           V(LLL) = SUPAR(I)
           K=4+NGLO
      60   DO 42 J=K,NPT
           J=JJ
           IF(V(LLL).LE.AEAT(JJ)) GO TO 56
           -2 CONTINUE
           IF(V(LLL).GE.AEAT(JJ)*3.) GO TO 65
      65   KJ = J-1
           K = KJ
           00 64 JJ=1,2
           IF(CPR(K).NE.0.) GO TO 63
           WRITE(6,62)K
           62 FORMAT(17H0CANNOT USE POINT,I2,3X,4HCP=0 )
           GO TO 1130
           63 PETC(JJ,T)=I.*T*CPR(K)*HNT(K)
           IF((EQL).PER(JJ,1)= PER(JJ,1)*DLVTP(K)
           PER(JJ,2)= TTI(K)/(E.*W4(K)*(HSUM(1)-HSUM(K)))
           RPP(JJ) = 1./((1.-/GAMMAS(K)-PER(JJ,2))
           IF(EQL)RPP(JJ) = 1.+DLVPT(K)+(1.-DLVTP(K))*PER(JJ,1)
           K = KJ + 1
           65 CONTINUE
           AMHT(LL) = WM(1)
           CALL SET(PPC(KJ),RP(1),AEAT(KJ),V(LLL),APCP(LL))
           CALL SET(TT(KJ),PER(1,1)*PCP(KJ),APCP(LL),AT(LL))
           IF(EQL)CALL SET(WMKJ),RPP(1),PCP(KJ),APCP(LL),AMHT(LL))
           K = KJ
           UC 74 JJ=1,2
           G(JJ,7)=SPINH(K)**2
           G(JJ+2,7)=2.*G(JJ,7)*PER(JJ,2)
           G(JJ+4,7)=(1.-GAMMAS(K))/GAMMAS(K)*G(JJ+2,7)
           G(JJ+1)=1.
           G(JJ+2,1)= 0
           G(JJ+3,1)=0
           G(JJ+2,2)=ALOG(PPC(K))
           G(JJ+2,2)=1.
           G(JJ+4,2)=0
           DO 70 N=3,6
           NXP=N-1
           GTJJ(M)=GT(JJ,2)**NXP
           NXP=NXP-1
           GTJJ(M)=G(JJ,2)**MXP*FLDAT(M-1)
           G(JJ+2,M)=G(JJ,2)**MXP*FLDAT(M-1)
           G(JJ+4,M)=G(JJ+2,M)/G(JJ,2)*FLOAT(M-2)
           70 CONTINUE
           K = KJ + 1
           76 CONTINUE
           IMAT = 6
           CALL MGAUSO
           AI(LLL)= X (1)
           DO 80 JJ=2,b

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           P1712 01835

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## SUBROUTINE RATIO FORTRAN EXTENDED VERSION 2.0

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      ATTEMPTALLY * X TJJ * ALG (APCP(LL))** (JJ-1)
      64 CONTINUE
      IF (AI(LL),LE,0.) GO TO 55
      AI(LL) = AI(LL)**.5
      GO TO 86
      85 LL = LL - 1
      86 WRITE(GEIT,DR,110) MARY(51)-TO 90
      LL = LL+1
      GO TO 1100
      115      C OUTPLT
      C
      C
      90 IF(EQ7) WRITE(6,187)
      120      87 FORMAT(1H1/20X,*THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING E
      1 EQUILIBRIUM COMPOSITION DURING EXPANSION*//)
      IF (.NOT. EQ7) WRITE (6,88)
      88 FORMAT(1H1/20X,* THEORETICAL GUN PROPELLANT PERFORMANCE ASSUMING F
      1 ROZEN COMPOSITION DURING EXPANSION*//)
      IF (.NOT. EQ8) WRITE (6,99)
      99 FORMAT (62X,28HAT AN ASSIGNED TEMPERATURE )
      WRITE (6,91)
      91 FORMAT (52X,24HFOR ASSIGNED AREA RATIOS //)
      PC = P(1)+14.696C06
      WRITE(6,191)PC
      130      191 FORMAT(5M10,2X,"(P0.1,9H PSIA)
      CALL OUT1
      IF (ISONIC.CQ,1) WRITE(6,33)
      33 FORMAT(16H0SUBSONIC FLOW //)
      IF (ISONIC.EQ.2) WRITE (6,35)
      35 FORMAT(16H0SUPERSONIC FLOW //)
      140      C AREA RATIC
      C
      C
      FMT(6)= FMT(8)
      FMT(4)= FMT(6)
      DO 92 M=1,LL
      K=2M+3
      145      FMT(K)= F3
      IF (V(M).GE.10.) FMT(K)=F2
      IF (V(M).LE.100.) FMT(K)=F1
      92 CONTINUE
      93 WRITE(6,FMT) FA1,FA2,F8,FB,(V(M),M=1,LL)
      150      C VACUUM SPECIFIC IMPULSE AND SPECIFIC IMPULSE
      C
      C
      00 93 M=1,LL
      V(M)=AI(M)+CSTR*V(M)/(32.174* APCP(M))
      93 CONTINUE
      155      FMT(4)=F4
      FMT(5)= F1
      WRITE(6,FMT) (FA(M),M=1,LL),
      WRITE(6,FMT) (FI(M),M=1,LL),
      WRITE(6,FMT) (FI(M),M=1,LL),
      WRITE(6,FMT) (AI(M),M=1,LL)
      160      P1712 01636
      P1712 01637
      P1712 01638
      P1712 01639
      P1712 01640
      P1712 01641
      P1712 01642
      P1712 01643
      P1712 01644
      P1712 01645
      P1712 01646
      P1712 01647
      P1712 01648
      P1712 01649
      P1712 01650
      P1712 01651
      P1712 01652
      P1712 01653
      P1712 01654
      P1712 01655
      P1712 01656
      P1712 01657
      P1712 01658
      P1712 01659
      P1712 01660
      P1712 01661
      P1712 01662
      P1712 01663
      P1712 01664
      P1712 01665
      P1712 01666
      P1712 01667
      P1712 01668
      P1712 01669
      P1712 01670
      P1712 01671
      P1712 01672
      P1712 01673
      P1712 01674
      P1712 01675
      P1712 01676
      P1712 01677
      P1712 01678
      P1712 01679
      P1712 01680
      P1712 01681
      P1712 01682
      P1712 01683
      P1712 01684
      P1712 01685
      P1712 01686
      P1712 01687
      P1712 01688
  
```

SUBROUTINE RATIO FORTRAN EXTENDED VERSION 2.0 31/12/70 08.09.56. PAGE NO. 5

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```

160      C
        C*
        C
        FMT(5) = FMT19
        DO 94 M=1,LL
        NV(M)=CSTR+5
165      CONTINUE
        WRITE(6,FMT) (FR1(N),N=1,6), (NV(N),N=1,LL)
        C
        CF - THRUST COEFFICIENT
170      C
        DO 95 M=1,LL
        V(PTEST17)+32.1757CSTR
175      CONTINUE
        FMT(5) = FB
        FMT(7) = F3
        WRITE(6,FMT) FC1,FB,FB,(V(N),N=1,LL)
        WRITE(6,96)
        WRITE(6,96)
        K=2*M+3
180      C
        PRESSURE RATIO
        C
        FMT(4) = FMT(6)
        DO 97 M=1,LL
        NV(M)=P(1)/APCP(M)
185      C
        FMT(K)=F3
        IF(APCP(M).GE.1000.) FMT(K)=F2
        IF(APCP(M).GE.10000.) FMT(K)=F1
        CONTINUE
190      C
        PRESSURE
        C
        WRITE(6,FMT) FR1,FB,FB,(APCP(M),N=1,LL)
        DO 98 M=1,LL
        K=2*M+3
        NV(M)=P(1)/APCP(M)
195      C
        FMT(K)=F3
        IF(V(N).GE.1.) FMT(K)=F3
        IF(V(N).GE.10.) FMT(K)=F2
        IF(V(N).GE.100.) FMT(K)=F1
        CONTINUE
200      C
        WRITE(6,FMT) (FF(N),N=1,6), (V(N),N=1,LL)
        C
        TEMPERATURE
        C
        DO 101 M=1,LL
        NV(M)=AT(M)+.5
101      CONTINUE
        FMT(5)=FMT13
        FMT(5)=FMT19
        WRITE(6,FMT) (FT(N),N=1,6), (NV(N),N=1,LL)
        C
        ENTHALPY
210      C
  
```

SUBROUTINE RATIO FORTRAN EXTENDED VERSION 2.0

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```

C
      FM1(5)= FB
      FM1(7)= F1
      DO 104 M=1,LL
      V1=M$UM(1)*R-1000.*CA1(M)/294.301**2
      104 CONTINUE
      WRITE(6,FMT1) (V1(N),N=1,LL)
      C
      C    ENTROPY
      C
      FM1(7)=F4
      V(1)= SSUM(2)*R
      224 0-106 N=1,LL
      V(M)= V(1)
      106 CONTINUE
      WRITE(6,FMT1) (FS(N),N=1,LL), (V(M),M=1,LL)
      C
      C    MOLECULAR WEIGHT
      C
      FM1(7)=F3
      WRITE(6,FMT1) (FM(N),N=1,LL), (AMNT(M),M=1,LL)
      110* CONTINUE
      120* CONTINUE
      RETURN
      END

```

SUBROUTINE REACT FORTQAN EXTENDED VERSION 2.0

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      P1712 0.1987
      P1712 0.1968
      P1712 0.1989
      P1712 0.1970
      P1712 0.1972
      P1712 0.1973
      P1712 0.1974
      P1712 0.1975
      P1712 0.1976
      P1712 0.1977
      P1712 0.1978
      P1712 0.1979
      P1712 0.1980
      P1712 0.1981
      P1712 0.1982
      P1712 0.1983
      P1712 0.1984
      P1712 0.1985
      P1712 0.1986
      P1712 0.1987
      P1712 0.1988
      P1712 0.1989
      P1712 0.1990
      P1712 0.1991
      P1712 0.1992
      P1712 0.1993
      P1712 0.1994
      P1712 0.1995
      P1712 0.1996
      P1712 0.1997
      P1712 0.1998
      P1712 0.1999
      P1712 0.2000
      P1712 0.2001
      P1712 0.2002
      P1712 0.2003
      P1712 0.2004
      P1712 0.2005
      P1712 0.2006
      P1712 0.2007
      P1712 0.2010
      P1712 0.2011
      P1712 0.2012
      P1712 0.2013
      P1712 0.2014
      P1712 0.2015
      P1712 0.2016
      P1712 0.2017
      P1712 0.2018
      P1712 0.2019

      COMMON/MISC/ENN,SUMN,IT,SD,ATOM(13,101),LLMT(15),SO(15),80P(15,2)
      1  *TH1,LCM,THIO,THIGH,PP,CPSUN,OF,EO(RAT),FPCT,R,RR,MSUB9,AC(2),AM(2)
      2  *HPP(2),RH(12),VMIN(12),VPLS(2),WP(12),DATA(22),NAME(15,5)
      3  *ANUM(15,5),PECHT(15),ENTH(15),FAZ(15),RTMP(15),DENS(15)
      *VHOM,MMW(15,7),TE,N,JANF

      COMMON/INDX/TOEBUG,CONVG,IP,HP,SP,HPPSP,TPSP,MOLES,NP,NT,NPT,L,NS,
      1  KHAT,IMAT,IG1-N,J,MONAT,IP,NEWR,NSUB,NSUP,IN,CPGVFR,CPGCEQ
      2  ,IONS,NC,NSERT,JSOL,ULIQ,KASE(14),NREAC,IC,IO2
      C   EQUIVALENCE (NAME,ANAME)

      DATA MOL/1HM/,0X/1HO/,LANK/1H /,IZERO/2HM/0/
      C   WRITE(16,3000)
      3000  FORMAT(1H *,REACTANTS*)
      DO 10 K=1,2
      - 24
      - M-HP(K)-st,
      HPE(K)*x0,
      RMCK(K)=0,
      VPLS(K)=0,
      VMIN(X)=0,
      AC(K)=0,
      ANH(K)=st,
      DO 8 J=1,15
      L1*(J,J)=0
      BOP(J,K)=0,
      80P(J,K)=0,
      6  CONTINUE
      10 CONTINUE
      30
      - 24
      - N=4
      L24
      NREAC=NREAC
      IF(NREAC.GT.16) NREAC=16
      DO 200 N=1,NREAC
      20  READ(5,21)(NAME(I,I),ANUM(I,I),I=1,5),PECHT(N),HOLE,ENTH(N),FAZ(N)
      21  FORMAT(5(A2,F7.5),F0XTN),DENS(NH)
      IF(NAME(N,1).EQ.LANK) GO TO 200
      IF(L.EQ.0) GO TO 20
      WRITE(16,311)(NAME(I,I),ANUM(I,I),I=1,5),PECHT(N),MOLE,ENTH(N),FAZ
      1 (N),RTMP(N),FOX(N),DENS(N)
      31  FORMATTXX-*T*2,1X,F7.4;2X,F9.4;2X,A1,F8.5,A1,F8.5)
      2A1,3X,F8.5)
      35  IF(MOLE.EQ.MOL) MOLES=.TRUE.
      K=2
      IF(FOX(N).EQ.0) X=1

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SUBROUTINE	REACT	FORTRAN EXTENDED VERSION 2.0	31/12/70	03.09.56.	PAGE NO.																									
55	DO 38 J=1,15 DATA(CJ) = 0. 39 CONTINUE RM=0. DO 100 JJ=1,5 IF(ANUM(N,JJ).EQ.0.)GO TO 101	IF(LLMT(JJ).EQ.0) CJ Y 45 IF(INAME(N,JJ).EQ.LLMT(JJ))GO TO 46 41 CONTINUE 45 L = NJ	P1712 02020 P1712 02021 P1712 02022 P1712 02023 P1712 02024 P1712 02025 P1712 02026 P1712 02027 P1712 02028 P1712 02029 P1712 02030 P1712 02031 P1712 02032 P1712 02033 P1712 02034 P1712 02035 P1712 02036 P1712 02037 P1712 02038 P1712 02039 P1712 02040 P1712 02041 P1712 02042 P1712 02043 P1712 02044 P1712 02045 P1712 02046 P1712 02047 P1712 02048 P1712 02049 P1712 02050 P1712 02051 P1712 02052 P1712 02053 P1712 02054 P1712 02055 P1712 02056 P1712 02057 P1712 02058 P1712 02059 P1712 02060 P1712 02061 P1712 02062 P1712 02063 P1712 02064 P1712 02065 P1712 02066 P1712 02067 P1712 02068 P1712 02069 P1712 02070 P1712 02071 P1712 02072	03.09.56.	2																									
60	DO 51 JEN,15 NJ = J IF(LLMT(JJ).EQ.0) CJ Y 45 IF(INAME(N,JJ).EQ.LLMT(JJ))GO TO 46 41 CONTINUE 45 L = NJ	46 DO 48 KK=1,131 IF(ATOM(1,KK).EQ.ANAME(N,JJ))GO TO 50 48 CONTINUE L=9 50 CC TO 20	51 RNM=ANUM(N,JJ) V1J=ATON(3,KK) DATA(CJ)=ANUM(N,JJ)	P1712 02032 P1712 02033 P1712 02034 P1712 02035 P1712 02036 P1712 02037 P1712 02038 P1712 02039 P1712 02040 P1712 02041 P1712 02042 P1712 02043 P1712 02044 P1712 02045 P1712 02046 P1712 02047 P1712 02048 P1712 02049 P1712 02050 P1712 02051 P1712 02052 P1712 02053 P1712 02054 P1712 02055 P1712 02056 P1712 02057 P1712 02058 P1712 02059 P1712 02060 P1712 02061 P1712 02062 P1712 02063 P1712 02064 P1712 02065 P1712 02066 P1712 02067 P1712 02068 P1712 02069 P1712 02070 P1712 02071 P1712 02072	03.09.56.	2																								
65	51 RNM=ANUM(N,JJ) V1J=ATON(3,KK) DATA(CJ)=ANUM(N,JJ)	52 PCNT=PCNT(N) IF(MOLFS) PCNT=PCNT*RH NP(K)=NP(K)+PCNT*V1J IF(INAME(N,5).NE.17ERO)HPP(K)=HPP(K)+ENTH(N)*PCNT/RM AM(K)=AM(K)+PCNT/R <sup>4</sup>	53 AM(K)=AM(K)+PCNT/R <sup>4</sup> DO 110 J=1,L BOF(J,K)=UATA(J)*PCNT/RM + HPP(J,K) 110 CONTINUE	54 IF(DENS(N).NE.0.7)GO TO 115 GO TO 117	55 115 RMCK(K)=RHO(K)*PCNT/DENS(N) 117 RMK(N) = RM	56 200 CONTINUE	57 IF(NREACS.LE.16) GO TO 1205 NRAC=NREACS+16	58 NRAC=NRAC+16 DO 1230 I=1,NRAC	59 1200 READ(5,21) JUNK	60 1205 IF(IL.EQ.0) GO TO 1000 IF(IL.EQ.0) GO TO 1000 DO 220 K=1,2	61 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	62 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	63 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	64 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	65 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	66 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	67 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	68 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	69 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	70 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	71 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	72 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	73 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	74 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	75 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	76 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	77 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	78 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	79 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2	80 220 IF(NU(K).EQ.0) GO TO 1000 IF(NU(K).EQ.0) GO TO 1000 DO 220 K=1,2
70	52 PCNT=PCNT(N) IF(MOLFS) PCNT=PCNT*RH NP(K)=NP(K)+PCNT*V1J IF(DENS(N).NE.0.7)GO TO 115 GO TO 117	81 100 CCNTINUE 101 PCNT=SPECWT(N) IF(MOLFS) PCNT=PCNT*RH NP(K)=NP(K)+PCNT*V1J IF(DENS(N).NE.0.7)GO TO 115 GO TO 117	82 110 CONTINUE	83 110 CONTINUE	84 110 CONTINUE	85 110 CONTINUE	86 110 CONTINUE	87 110 CONTINUE	88 110 CONTINUE	89 110 CONTINUE	90 110 CONTINUE	91 110 CONTINUE	92 110 CONTINUE	93 110 CONTINUE	94 110 CONTINUE	95 110 CONTINUE	96 110 CONTINUE	97 110 CONTINUE	98 110 CONTINUE	99 110 CONTINUE	100 110 CONTINUE									

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  IF(POX(N).EQ.0) GO TO 210
  IF(POX(N).NE.0 AND K.EQ.1) GO TO 210
  PECNT(N) = PECWT(N)/NP(K)
  210 CONTINUE
  220 CONTINUE
  NEWR=.TRUE.
  220 N=1NREAC
  IF (DENS(N).NE.C) GO TO 230
  RHC(1)=0.
  GO TO 1000
  230 CONTINUE
  1000 RETURN
  END

```



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SUBROUTINE RK7OUT FORTRAN EXTENDED VERSION 2.0      31/12/70      06.09.50.
      C PRESSURE RATIOS      P1712 02140
      55      C DO 45 I=1,NPT      P1712 02140
      K= 2*I+3      P1712 02140
      FMT(K)= F3      P1712 02140
      IF (PCP(I).GE.1000.) FMT(K)=F2      P1712 02140
      IF (PCP(I).LT.1000.) FMT(K)=F1      P1712 02140
      IF (PCP(I).GE.130000.) FMT(K)= F0      P1712 02140
      45 CONTINUE      P1712 02140
      WRITE (6,FMT) FR1,FB,FB,(PCP(J),J=1,NPT)      P1712 02140
      CALL OUT2      P1712 02140
      65      C AGV = 9.00655      P1712 02140
      DO 202 K=2,NPT      P1712 02140
      SPIN(K) = (2.*RR*(HSUM(1)-HSUM(K))**5./AGV      P1712 02140
      C - AN (A/M) IN UNITS OF SEC/ATM      P1712 02140
      70      C AN = RR*TTT(K)*SPIN(K)**2      P1712 02140
      IF (K.NE.2) GO TO 201      P1712 02140
      AN=AN      P1712 02140
      CSTR=32.174*P(1)*ANT      P1712 02140
      75      201 AEAT(K)=AN/ANT      P1712 02140
      VAC(K)=SPIN(K)+PPP(K)*AN      P1712 02140
      IF (SONVEL(K).NE.0.) VMOC(K)=SPIN(K)*AEAT(K)      P1712 02140
      NV(K)= CSTR + .5      P1712 02140
      80      202 CONTINUE      P1712 02140
      C MACH NUMBER      P1712 02140
      83      C VMOC(K)=0.      P1712 02140
      85      IF (GAMMAS(2).EQ.0.) VMOC(2)=0.      P1712 02140
      FM(7)= F3      P1712 02140
      WRITE(6,FM(7))(FN(I),I=1,4),(VMOC(J),J=1,NPT)      P1712 02140
      C VELOCITY      P1712 02140
      90      C DO 1202 I=1,NPT      P1712 02140
      SONVEL(I)=VMOC(I)*3.260840      P1712 02140
      1202 CONTINUE      P1712 02140
      WRITE(6,1203)(VELOC(I),I=1,NPT)      P1712 02140
      1203 FORMAT(1H,*VEL, FT$SEC *13F9.1)      P1712 02140
      CALL VISCONT(NP,T,SUSTEM,TON,TTT)      P1712 02140
      IF (FLAGGG.GT.0) GO TO 203      P1712 02140
      C CONSTANT VOLUME AND IMPETUS      P1712 02140
      100      C IVOLUME=VOLUME*.5      P1712 02140
      WRITE(6,100) IVOLUME*IMPETUS      P1712 02140
      9000 FORMAT(1H,*T, CV, OEG K*,6X,15/1H ,*1NPETUS      P1712 02140
      203 WRITE(6,206)      P1712 02140
      206 FORMAT(1H )      P1712 02140
      105      C

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SUBROUTINE RKOUT FORTRAN EXTENDED VERSION 2.0

      C   C
      C   FMT(4) = FMT9X
      C   FMT(5) = FMT13
      C   FMT(6) = FMT19
      C   FMT(7) = F8
      C   WRITE(*,FMT(FRTR(I),I=1,4)) * (WVCTJ,J)
      C   CF - THROUET COEFFICIENT
      C   FMT(6) = FMT(8)
      C   FMT(7) = F3
      C   DO 212 I=2,NPT
      C   212 V(I)=3*74*SPIM(I)/CSTR
      C   WRITE(6,FMT)FC1,FB,FB,(V(J),J=2
      C   AREA RATIO
      C   FMT(5)=FB
      C   DO 214 I = 2,NPT
      C   214 K=2*I-3
      C   FMT(K)=F4
      C   IF (AEAT(I).GE.1.) F4*T(K) = F3
      C   IF (AEAT(I).GE.10.) FMT(K) = F2
      C   214 CONTINUE
      C   IF (TREAT(I).GE.100.7) FNT(K) = F1 -
      C   WRITE(*,FMT)FA1,FA2,FB,FR,(AEAT(I))
      C   VACUUM IMPULSE
      C   FMT(5)=FMT13
      C   FMT(7)=F1
      C   WRITE(6,FMT)(FA(I),I=1,4),(VACI(I),
      C   SPECIFIC IMPULSE
      C   WRITE(*,FMT(FRTR(I),I=1,4),TSPIK(J))
      C   WKITE(6,208)
      C   FMT(4) = F9
      C   FMT(5) = FMT13
      C   FMT(7) = F5
      C   IF (EOL) GO TO 312
      C   WRITE(6,310)
      C   310 FORMAT(15HOMOLE FRACTIONS //)
      C   MOLE FRACTIONS - FROZEN
      C   LINE = 0
      C   DO 457 K = 1,NS
      C   VALINE+1) = SN(K,1)/TOTN(1)
      C   IF (VALINE+1).LT.(5.E-6) GO TO 42
      C   LINE = LINE+1
      C   21LINE,I) = SUB(K,1)

```

## SUBROUTINE RKTOUT FORTRAN EXTENDED VERSION 2.0

```

160      Z(LINE,2) = '3(K,2)
          Z(LINE,3) = SUB(K,3)
          Z(LINE,4) = V(LINE)
424      IF (LINE.NE.4.AND.K.NE.NS) GO TO 430
          IF (LINE.EQ.0) GO TO 312
          WRITE (6,426) (Z(LN,1),Z(LN,2),Z(LN,3),Z(LN,4),LINE)
426      FORMAT (TM,4F3.4,F9.5,TX)
          LINE = 0
430      CONTINUE
          312 CALL OUT3
170      100n RETURN
          END

```



SUBROUTINE ROCKET FORTRAN EXTENDED VERSION 2.0 31/12/70 08:09:56. PAGE NO: 2

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55      GO TO 311
      396 NP = 2
      DO 310 I=1,24
      IF (I.GT.2) GO TO 309
      IF ((PCP(1).EQ.0.) OR .PCP(1).EQ.1.) GO TO 310
      309 IF ((PCP(1).EQ.0.) GO TO 311
      NP = NP + 1
      PCP(NP) = PCP(1)/PCP(1)
      310 CONTINUE
      311 NSUB=0
      NSLP = 0
      DO 320 I=1,13
      IF (NSUP(1).NE.0.) NSUB=NSUP+1
      320 CONTINUE
      WRITE (6,9KTINP)
      SS0 = 0.
      ITROT= 3
      ITT = ITT+1
      C
      C SET ASSIGNED P
      75      C
      DO 902 IP = 1,NP
      PP = P(IP)
      CATE-COMBIN
      T(NPT) = TT
      IF (TT.NE.0.) GO TO 333
      IF (NPT.EQ.0) GO T3 1.000
      GO TO 900
      333 PCP(NPT) = P(1)/PP
      IT-IP-OT-TT--GO TO 295
      87  65      C
      C COMBUSTION CHAMBER
      C
      TP = .FALSE.
      MP = .FALSE.
      SP = .TRUE.
      S0 = SSUM(1)
      FG*(2)=((GAMMAS(1)+1.)/2.)*(GAMMAS(1)/(GAMMAS(1)-1.))
      P(2) = P(1)/PCP(2)
      TT = 2.*TT/(GAMMAS(1)+1.)
      GO TO 900
      295 IT-IP-OT-TT--GO TO 900
      C
      C THROAT
      C
      190 IF (ITH.NE.2) GO TO 191
      ITTH = 1
      GAMMAS(2)=0.
      191 OH = HSUM(1)-HSUM(2)
      OHSTAR = OH-GAMMAS(2)*IT*ENN/2.
      IF (IGERUG) WRITE (6,923) OHSTAR,HSUM(1),HSUM(2),PCP(2)
  
```



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SUBROUTINE SEARCH FORTRAN EXTENDED VERSION 2.0

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SCEROUTINE SEARCH

C SEARCH TAPE FOR THERMO DATA FOR SPECIES TO BE CONSIDERED  
C INTEGER S19,OMIT,EN,

05 C LOGICAL NEWR

```
      C DIMENSION DATE(2,3),MT(4),B(4), OMIT(3,3)
      C COMMON/SPECES/CCEF(2,7,150),S(150),EN(150),ENLN(150),H0(150)
      1  *CELN(150),A(15,150),SUB(150,31),IUSE(150),TEMP(150,2),
      COMMON/MISC/ENN,SUMM,TIT,SU,AUTOM(3,31),LLMT(15),BD(15,2)
      1  *TM,TLW,TMIC,THIC,PP,GSUM,DF,EGRAT,FPCT,R,RR,HSUDJ,AC(2),AM(2),
      2  *HOP(12),RHO(12),W4IN(2),VPLS(2),WP(12),DATA(22),NAME(15,5)
      3  *ANU(15,5),PECH(115),ENTH(115),RTEMP(115),FCX(15),DENS(15),
      4  *RHO,P,RH(115),TLN,JANF
      COMMON/INDX/IDEBUG,CONVG,TP,HPS,SP,HPS,TPSP,MOLES,NP,NT,L,NS,
      1  KMAT,IMAT,IQ1,N,J,NOMIT,IP,NEWR,NSUB,NSUP,ITA,CPGVFR,CPGVTO
      2  ,TONS,TC,INSERT,DSOL,JCJU,TRSET,IQ2,NREAC,IC,IC,IQ2
      20 C EQUIVALENCE (DATE,EN),(OMIT,ENLN),(ENDD,END)
      C DATA GAS/IHG/,END/3HEND/
      C
      25 NC=0
      1A=0
      COEF(1,1,1)=END
      DC 3 I=1,150
      ISAVE=I
      IF(A(1,1,1).EQ.END) GO TO 4
      -90
      30 00 3 J=1,1
      A(J,I)=0.
      * CONTINUE
      4  MAXNS=ISAVE
      REMND 9
      READ (19,5) TLW,TMID,THIGH
      35
      9 FORMAT(TOPIC,3)
      NS = 1
      7 READ (19,10) (SUB(NS,I),I=1,3),DATE(1,NS),MT(J),G(J),
      1  J=1,4),PHAZ(1,1,T2)
      10 FORMAT(3A4,5X,2A3,(A2,F3.3))
      IF(SUB(NS,1).EQ.END) GO TO 171
      READ (19,20) (TOPIC,17,NS),J,NS,1,2
      20 SUMAT (SE15,6)
      IF(NOMIT.EQ.0) GO TO 610
      00 605 I=1,NOMIT
      00 804 J=1,3
      IF(OMIT(I,J).NE.SUB(NS,J)) GO TO 605
      50
      804 CONTINUE
      610 GO TO 7
      805 CONTINUE
      610 DO 820 K=1,4
      IF(B(K).EQ.0.) GO TO 825
      P1712 02416
      P1712 02417
      P1712 02418
      P1712 02419
      P1712 02420
      P1712 02421
      P1712 02422
      P1712 02423
      P1712 02424
      P1712 02425
      P1712 02426
      P1712 02427
      P1712 02428
      P1712 02429
      P1712 02430
      P1712 02431
      P1712 02432
      P1712 02433
      P1712 02434
      P1712 02435
      P1712 02436
      P1712 02437
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      P1712 02439
      P1712 02440
      P1712 02441
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      P1712 02458
      P1712 02459
      P1712 02460
      P1712 02461
      P1712 02462
      P1712 02463
      P1712 02464
      P1712 02465
      P1712 02466
      P1712 02467
      P1712 02468
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      DO 105 IT=1,L
      IF(1.LM(I).EQ.MI(K)) GO TO 620
  55      168  CONTINUE
          DO 619 J=1,L
          619  A(J,NS) = 0.
          GO TO 7
  66      820  ATTEMPT-BTKY
          825  IF(NS.EQ.MAXNS) GO TO 870
          IUSE(NS)= 0
          IF(PH2.EQ.GAS) GO TO 170
          NC= NC-1
          TEMP(NC,1)= T1
          TEMP(NC,2)= T2
          IX= IX+1
          IF(IUSE(NS-1).EQ.0 .OR. NC.EQ.1) GO TO 145
          DO 830 I=1,L
          830  IF(A(I,NS).NE.A(I,NS-1)) GO TO 145
  70      A30  CCONTINUE
          IX= IX-1
          145 IUSE(NS)= -IX
  170  NS= NS+1
          GO TO 7
  75      970  WRITE(6,871) {SUBINS,J},J=1,3
          871  FORMAT(45MDIMNS,IN/SPECES/TOO SMALL TO CONSIDER ,3A4)
          GO TO 7
  171  NS= NS-1
          NEHR= .FALSE.
          WRITE(6,172)
  172  FORMAT(42H0 SPECIES BEING CONSIDERED IN THIS SYSTEM )
          DO 174 I=1,NS,5
  174  IX= IX+4
  85      IF(NS.LT.15) IS=NS
          174  WRITE(6,176) (DATE(I,J),SUB(I,J,1),SUB(I,J,2),SUB(I,J,3),J=1,
  1    15)
          176  FORMAT(5(5X,2A3,2X,3A4))
          RETURN
          END

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## SUBROUTINE SET FORTRAN EXTENDED VERSION 2.0

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SUBROUTINE SET FORTRAN EXTENDED VERSION 2.0
      C
      C USED FOR AREA RATIO INTERPOLATION ONLY
      C SETS UP ALL 4 BY 5 MATRICES
      05
      C
      C DOUBLE PRECISION A,ANS,G,X
      C
      C DIMENSION ANS(6),UNE(2),THD(2),THREE(2),A(20,21)
      C
      C COMMON/DOUBLE/G(20,21),X(20),
      C COMMON/IDEGUS/ IDEGS,IP,HP,SP,HPS,TPSD,MOLES,NP,NT,NS,
      1   A(MAT,IMAT,IG1,N,J,NOMIT,IF,NEWR,NSUP,INTN,CPGVFR,CPGVEQ
      2   TIONSTHRSERT,JSOL,JLIQ,KASE(14),NREAC,IC,IO2
      C
      C EQUIVALENCE (G,A),(X,ANS)
      C
      C DO 8 J=1,2
      C     A(J,5)=ALCG(ONE(J))
      C     ATJ=2+5*(J-1)
      C
      20    A(J,2)=ALOG(THREE(ATJ))
      6    CONTINUE
      00 1   I=1,2
      A(I,1)=2.0
      A(I+2,1)=6.9
      A(I+2,0)=0.0
      ATI=2+2*(I-1)+0
      25    DO 1 J=2,3
      A(I,J+1)=A(I,2)**J
      MXP=J-1
      A(I+2,J+1)=A(I,2)**MXP*FLOAT(J)
      30    1  CONTINUE
      IMAT = 3
      CALL MGAUSD
      HAL=ANS(1)
      SUM=MALOG(ARG)
      35    DO 10 J=1,3
      HAL=HAL+SUM**J*(ANS(J+1))
      40    10  CONTINUE
      HAL=EXP(HAL)
      RETURN
      END

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## SUBROUTINE VISCON FORTRAN EXTENDED VERSION 2.0

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C 09.56.

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--&gt; SUBROUTINE VISCON(NS,NPI,SUB,EN,TOTN,T)

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C THIS SUBROUTINE COMPUTES THE VISCOSITY AND THE CONDUCTIVITY
C OF A GAS MIXTURE CONSISTING OF 5 GASEOUS SPECIES.
C GASEOUS SPECIES TO BE CONSIDERED ARE H2O,CO,H2,CO2,AND N2.
C
C COMMON/PERCENT/FMOLE
DIMENSION SUB(150,3),EN(150,13),TOTN(13),T(13),SPECIE(5),EK(5).
1SIG(5),NGTH(5),TE(33),OME(G(33),FMOLE(5),VIS(5),COND(5).
2VISMAX(13),COMMX(13)
DATA (SPECIE(I),I=1,5)/4HH20 *4HH20 *4HH20 *4HH20 *4HH20 /
DATA (SIG(I),I=1,5)/2.824,3.706,2.915,3.897,3.749/
DATA (TE(I),I=1,5)/2.230,9.85,0.36,0.2,2.3,0.79,87/
DATA (NGTH(I),I=1,5)/16,26,01,2.016,44.01,26,02/
DATA (OMEG(I),I=1,5)/0.03026693,0.35019891,0.35355339059/
DATA (CEN2,CON2,COWS/,0.03026693,0.35019891,0.35355339059/
DATA (TE(I),I=1,3)/1.0,1.2,1.4,1.6,1.8,2.0,2.2,2.4,2.6,2.8,3.0,
13.2,1.4,1.6,3.0,4.5,5.0,6.0,7.0,8.0,9.0,10.0,11.0,12.0,13.0,14.0,
215.0,16.0,32.0,64.0,128.0,256.0,512.0/
DATA (TOTN(I),I=1,13)/1.5918,1.4588,1.3557,1.2998,1.2216,1.21751,
21 1.1377,1.1056,1.063,1.0579,1.0385,1.0214,1.0063,0.9928,0.9807,
25.9696,0.9265,0.966,0.8725,0.8536,0.8376,0.8242,0.8123,0.8017,
30.7922,0.7436,0.7756,0.7883,0.6939,0.6262,0.5634,0.5056,0.4526/
C VALUES FOR VISCOSITY AND CONDUCTIVITY WILL BE COMPUTED AT THE
C CHAMBER, THE THROAT, AND AT THE ASSIGNED EXIT.
C
C WRITE(6,8999) NS,NPT
8999 FORMAT(2I10)
  PMLE=0.0
  DO 1000 M=1,NPT
  10
C COMPUTE THE MOLE FRACTIONS OF THE 5 GASEOUS SPECIES.
C
C 00 20 I=1,5
  20 J=1,NS
  30
C SEARCH THE ARRAY SUB(J,1) FOR THE 5 NEEDED SPECIES. WHEN ONE OF THE
C NEEDED SPECIES IS FOUND, COMPUTE THE MOLE FRACTION.
C
C IF(SPECIE(I).NE.SUB(J,1)) GO TO 10
  40
  FMOLE(I)=EN(J,M)/TCVN(M)
  WRITE(6,9000) SPECIE(I),SUB(J,1),EN(J,M),TOTN(M),FMOLE(I),J,M
  45
  9000-FORMAT(4X,2A10,3F15.8,3I5)
  IF(H.EQ.1) FMOLE=FMOLE+FMOLE(I)*100.
  GO TO 20
  10 CONTINUE
  C IF THE SPECIE CANNOT BE LOCATED IN THE ARRAY SUB(J,1). SET THE MGLE
  C FRACTION TO MINUS ONE.
  C
  50   FMOLE(I)=-1.0
  20 CONTINUE
  C COMPUTE THE VISCOSITY AND THE CONDUCTIVITY FOR EACH OF THE 5 SPECIES P171201 00062

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      SUBROUTINE VICON FORTRAN EXTENDED VERSION 2.0

  55      C          DO 100 I=1,5
           IF(FMOLE(I).LT.0.0) GO TO 100
           TEK=T(M)/EK(I)
           IF(TEK.LT.TE(1)) TEK=TE(1)
           IF(TEK.GT.TE(33)) TEK=TE(33)
           DO 40 J=1,33
           IF(TEK-TE(J)) 30,25,40
           25  DCM=ONEG(J)
           GO TO 50
           30  FRAC=((TEK-TE(J-1))/(TE(J-1)-TE(J)))
           DCN=DCM*(J-1)+FRAC*(DCM*(J-1)-ONEG
           TCC TO 50
           40  CONTINUE
           50  GIV=SIG(I)*SIG(I)*D04
           C          VISMIX=CONI*SCRT(GTM(I))*VIS(I)/DIV
           C          CONDUCTIVITY
           C          CONDI=CCN2*SQRT(T(M)/WGT(M))/DIV
           C          WRITE(6,9001) T(M),EK(I),TEK,TE(J-1),
           C          10IV,UCN,SIG(I),GTM(I),VIS(I),COND
           C          9001 FORMAT(6F15.6,7F15.6,3I5)
           100  CONTINUE
           C          COMPUTE VISCOSITY AND CONDUCTIVITY
           C          VISMIX=M=0.0
           CONMIX(M)=0.0
           DO 200 I=1,5
           SUM=0.0
           IF(FMOLE(I).LT.0.0) GO TO 200
           200 150  J=1,5
           IF(FMOLE(J).LT.0.0) GO TO 150
           F1=SOR(T1,MGT(M)/WGT(M))
           F2=SOR(VIS(I)/VIS(J))
           F3=INGTM(J)/WGT(M))
           FA=1.+F2*F3
           FAC=CONS/F1
           FA=FAC*FA*FA
           SUM=SUM+FMOLE(I)*PHI
           WRITE(6,9002) FMOLE(I),FMOLE(J),WGT
           C          1F2,COND(I),COND(J),F3,FA,FAC,PHI,S
           9002 FORMAT(6F15.6,7F15.6,3I5)
           150  CONTINUE
           C          VISCOSITY OF MIXTURE
           C          VISMIX=M=VISMIX(M)+FMOLE(I)*VIS(I)
  100
  105

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SUBROUTINE	VISCON	FORTRAN EXTENDED VERSION 2.0	31/12/70	08.09.56.	PAGE NO. 2
55	C	DO 100 I=1,5 IF (FMOLE(I).LT.0.0) GO TO 100 TEK=I(M)/EK(I) IF (TEK.LT.1E-11) TEK=TE(1) IF (TEK.GT.1E-333) TEK=TE(333) DO 400 JEX=1,33 IF (TEK-TE(J)) 30,25,40 25 DCP=OMEG(J), GO TO 50 30 FRAC=(TEK-TE(J-1))/(TE(J-1)-TE(J)) DCP=OMEG(J-1)+FRAC*(OMEG(J-1)-OMEG(J)) 40 GOTO 50 40 CONTINUE 50 GIV=SIG(I)*SIG(I)*D04		P171201 00063 P171201 00054 P171201 00065 P171201 00066 P171201 00067 P171201 00068 P171201 00069 P171201 00070 P171201 00071 P171201 00072 P171201 00073 P171201 00074 P171201 00075 P171201 00076 P171201 00077 P171201 00078 P171201 00079 P171201 00080 P171201 00081 P171201 00082 P171201 00083 P171201 00084 P171201 00085 P171201 00086 P171201 00087 P171201 00088 P171201 00089 P171201 00090 P171201 00091 P171201 00092 P171201 00093 P171201 00094 P171201 00095 P171201 00096 P171201 00097 P171201 00098 P171201 00099 P171201 00100 P171201 00101 P171201 00102 P171201 00103 P171201 00104 P171201 00105 P171201 00106 P171201 00107 P171201 00108 P171201 00109 P171201 00110 P171201 00111 P171201 00112 P171201 00113 P171201 00114 P171201 00115	
60	C	VISIT=COND*SQRT(WGTM(I))+VVIS(I)/DIV			
65	C	COND(I)=SCN2*SQRT(T(M)/WGTM(I))/DIV WRITE(6,9001) T(M),EK(I),TE(J-1),TE(J),FRAC,OMEG(J-1),OMEG(J), C IDIV,WGM(STIG(I),WGTM(I)),VISIT,COND(I),I,J,M C 9001 FORMAT(6F15.6,6F15.8,3I5)			
70	C	VISCOSITY			
75	C	CONDUCTIVITY			
80	C	COMPUTE VISCOSITY AND CONDUCTIVITY OF MIXTURE.			
85	C	VISMIX(M)=0.0 CONDIX(M)=0.0 DO 200 I=1,5 SUM=0.0 IF (FMOLE(I).LT.0.0) GO TO 200 DO 150 J=1,5 IF (FMOLE(J).LT.0.0) GO TO 150 F1=SORT(I)+WGTM(I)/WGTM(J)) F2=SORT(VIS(I)/VIS(J)) F3=(WGTM(J)/WGTM(I))*10.25 FA=1.*F2*F3 FAC=CONS/F1 PHI=FACT*FA			
90	C	SUM=SUM+FMOLE(J)*PHI WRITE(6,9002) FMOLE(I),WGTM(J),WGTM(I),VIS(I),VIS(J), C 1F2,COND(I),COND(J),F3,FA,FAC,PHI,SUM,I,J,M C 9002 FORMAT(6F15.6,7F15.6,3I5)			
100	C	150 CONTINUE			
95	C	VISCOSITY OF MIXTURE			
105	C	VISMIX(M)=VISMIX(M)+FMOLE(I)*VIS(I)/SUM			

SUBROUTINE VISCON FORTRAN EXTENDED VERSION 2.0  
 C CONDUCTIVITY OF MIXTURE  
 C  
 110 C CONMIX(M)=CONMIX(M)+FMOLE(I)\*COND(I)/SUM  
 C WRITE(6,9009) VISMIX(M),CONMIX(M),N  
 9009 FORMAT(1X,2F15.11,3X,15)  
 200 CONTINUE  
 100H CONTINUE  
 WRITE(6,2010) (VISMIX(I),I=1,NPT)  
 WRITE(6,2010) (CONMIX(I),I=1,NPT)  
 2000 FORMAT(1H ,\*VISC, GCM-SEC\*,13F9.6)  
 210H FORMAT(1H ,\*C, CAL/G-SEC^K\*,13F9.6)  
 RETURN  
 ENC

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APPENDIX II  
POLYNOMIAL FIT PROGRAM

97  
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PROGRAM SLSQF (INPUT,OUTPUT),  
 DIMENSION TT(100),CPR(100),HTR(100),STR(100),  
 CCHR(100),CHTR(100),CSR(100),  
 NPT(2),NAME(6),  
 CCHON/MATRIX G(10,10),X(10),IMAT  
 R=1-9.6726  
 ASSIGN 500 TO MEOF  
 IFEOF(MEOF) 500,500,1  
 1 READ 43,JHO,NPT,NAME  
 46 FCRNAT(F10.1,2I3,5X,6A10)  
 FRNT 112,NAME,HO  
 242-FCRNAT((1H1,29X,6A14)/1P,5HNO = ,F10.1//)  
 K7=0  
 111 KPT=NPT+1  
 NVAL=NPT(KPT)  
 READ 6,IT1(K),K=1,NVAL  
 READ 7,(CPR(K),K=1,NVAL)  
 PEG-7,(HTR(K),K=1,NVAL)  
 DC 22 I=1,NVAL  
 22 HRI(I)=HTR(I)+1000.♦HO  
 READ 7,ISTR(K),K=1,NVAL  
 6 FSRMAT(20F4.0)  
 7 FCRMAT(10F8.3)  
 25 DC 36 I=1,10  
 0 C 15 J=1,11  
 C(I,J)=0.  
 15 CONTINUE  
 16 CCNTINUE  
 SLH1=0.  
 19 SUMT2=0.  
 SUMT3=0.  
 SUMT4=0.  
 SUMT5=0.  
 SUMT6=0.  
 SUMT7=0.  
 SUMT8=0.  
 SUMT9=0.  
 SUMT10=0.  
 DO 200 K=1,NVAL  
 1=TT(K)  
 43 C=CPR(K)/R  
 H1=HTR(K)/(R\*T)  
 S1=STR(K)/R  
 TLOG=ALOG(T)  
 T2=T\*\*2  
 T3=T2\*T  
 T4=T3\*T  
 T5=T4\*T  
 T6=T5\*T  
 T7=T6\*T  
 T8=T7\*T  
 T9=T8\*T  
 T10=T9\*T  
 T11=T10\*T  
 T12=T11\*T  
 T13=T12\*T  
 T14=T13\*T  
 T15=T14\*T  
 T16=T15\*T  
 T17=T16\*T  
 T18=T17\*T  
 T19=T18\*T  
 T20=T19\*T  
 T21=T20\*T  
 T22=T21\*T  
 T23=T22\*T  
 T24=T23\*T  
 T25=T24\*T  
 T26=T25\*T  
 T27=T26\*T  
 T28=T27\*T  
 T29=T28\*T  
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 T32=T31\*T  
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 T161=T160\*T  
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## SLSQF FORTRAN EXTENDED VERSION 2.0

SUM12=SUM12+T2

SUM13=SUM13+T3

SUM14=SUM14+T4

SUM15=SUM15+T5

SUM16=SUM16+T6

SUM17=SUM17+T7

SUM18=SUM18+T8

SLMT2=SUMTM2+TM2

G(1,1)=G(1,1)+2.\*TLOG\*\*2

G(1,2)=G(1,2)+(1.5\*TLOG)\*T

G(1,3)=G(1,3)+(4./3.+5\*TLOG)\*T2

G(1,4)=G(1,4)+(1.25\*TLOG/3.)\*T3

G(1,5)=G(1,5)+(1.2\*TLOG/4.)\*T4

G(1,6)=G(1,6)+TREC

G(1,7)=G(1,7)+TLOG

G(1,11)=G(1,11)+CP+HT+ST\*TLOG

G(2,1)=G(2,11)+(CP+.5\*HT+ST)\*T

G(3,1)=G(3,11)+(CP+HT/3.+.5\*ST)\*T2

G(4,1)=G(4,11)+(CP+HT/4.+ST/3.)\*T3

G(5,1)=G(5,11)+(CP+HT/5.+ST/4.)\*T4

G(6,1)=G(6,11)+HT\*TREC

G(7,1)=G(7,11)\*ST

IF(X.GT.1) GO TO 50

G(1,8)=J

G(1,9)=1.0

G(2,6)=FLOAT(INVAL)/2.0

G(2,8)=T

G(2,9)=1/2.0

G(3,10)=12

G(3,9)=12/3.

G(4,8)=2

G(4,9)=T3/4.

G(6,10)=T3/3.

G(5,2)=T4

G(5,3)=14/5.

G(5,10)=T4/4.

G(6,9)=TREC

G(7,7)=FLOAT(INVAL)

G(7,4)=0.85,0

G(8,11)=CP

G(9,11)=HT

G(10,11)=ST

50 CCNTINUE

100 CCNTINUE

G(2,4)=2.13.19./4.+SUM12

G(2,3)=(5./3.)\*SUM13

G(2,4)=(35./24.)\*SUM14

G(2,5)=(27./20.)\*SUM15

G(2,7)=SUM17

G(3,3)=(49./36.)\*SUM14

## PROGRAM SLSQF FORTRAN EXTENDED VERSION 2.0

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1546.06.

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      G(3,4)=(5./4.)*SUM15
      G(3,5)=(143./120.)*SUM16
      G(3,6)=SUM17/3.
      G(3,7)=SUM12/2.
      G(4,4)=(169./144.)*SUM16
      G(4,5)=(47.-45.)*SUM17
      G(4,6)=SUM12/4.
      G(4,7)=SUM13/3.
      G(5,5)=(441./400.)*SUM16
      G(5,6)=SUM13/5.
      G(5,7)=SUM14/4.
      G(6,6)=SUM12/4.
      DO 200 J=1,10
      DC 210 J=I,10
      IF(I.EQ.J) GO TO 210
      6(W,I)=S(I,J)
      210 CONTINUE
      .00--CONTINUE
      125 PRINT 92
      IF(DEBUG(1).NE.0.) GO TO 190
      92 FORMAT(1H ,*VALUES OF G*)
      DO 90 I=1,10
      PRINT 91,(G(I,J),J=1,11)
      91 FORMAT(1X,1E15.0/1X,3E15.0)
      90 CONTINUE
      190 IMAT=10
      CALL MGAUSO
      PRINT 94
      94 FORMAT(1H ,*COEFFICIENTS ARE*)
      95 PRINT--192,X
      192 FORMAT(1X,7E15.0/1X,3E15.0)
      UC 401 I=1,NVAL
      T=TT(1)
      T2=T*T
      T3=T2*T
      T4=T3*T
      TLOG=ALOG(T)
      CCP5(I)=X(1)+X(2)*T+X(3)*T2+X(4)*T3+X(5)*T4
      CCP6(I)=CCP5(I)*R
      CTR(I)=((X(1)+X(2)*T/2.+X(3)*T2/3.+X(4)*T3/6.+X(5)*T4/5.)*T+X(6))
      1*K
      CTR(I)=CTR(I)-W0/1000.
      CSIR(I)=(X(1)*TLOG+X(2)*T+X(3)*T2/2.+X(4)*T3/3.+X(5)*T4/4.+X(7)
      1R
      400 CONTINUE
      PRINT 401
      401 FORMAT(1H ,*      CP      CCP      HT      CHT      T      :ST
      155   50 410 I=1,NVAL
      CCP7=ABS(CCP(I))-CCP(I)
      D1R=(INT(I1)-I0)/1000.
      D2R=ABS(D1R-CHTR(I))
      OSTR=ABS(STR(I)-CSIR(I))

```

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160					
	411	FORMAT(1H ,1X,'%D.%E')			
	1CMT,OSTR	PRINT(411,TT(I)),CPA(I),CCPK(I),STR,I,CHR(I),STR(I),CSTR(I),DCPK,			
	410	CCHTINUE			
		GC TO (111,1),KPT			
	165	500 CCHTINUE			
		END			

## SUBROUTINE MGAUSD FORTAN EXTENDED VERSION 2.0

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## SUBROUTINE MGAUSD

C SOLVE ANY LINEAR SET OF UP TO 20 EQUATIONS

05 C DOUBLE PRECISION G,X,COEFX(20),SUM,Z  
C DIMENSION COEFX(20)

C COMMON/MATRIX/ G(10,11),X(10),IMAT

10 C EQUIVALENCE (IUSE,IMAT)

10 C DATA BIGNO/1.E+38/

DATA BIGNO/1.E+320/

15 C BEGIN ELIMINATION OF NTH. VARIABLE

IUSE1=IUSE+1

6 DC-45&gt;NN=1,IUSE

IF (NN-IUSE) 8,3,6

20 83 IF(G(NN,NN))31,23,31

C SEARCH FOR MAXIMUM COEFFICIENT IN EACH ROW

C 4 DC-48 I=NN,IUSE

C COEFX(I) = BIGNO

IF(I,NN).EQ.0.) GO TO 16

C COEFX(I) = 0.

DO 10 J=NN,IUSE1

SUM = G(I,J)

IF(SUM.LT.D) SUM=SUM

IF(J,NE,NN) GO TO 9

2 = SUM

GO TO 10

9 IF(SUM.GT.COEFX(I)) COEFX(I)=SUM

10 CONTINUE

TEMP = BIGNC

I=0

20 DO 22 J=NN,IUSE

IF (COEFX(W)-TEMP) 87,22,22

A7 TEMP=COEFX(W)

I=J

22 CONTINUE

IF(I) 20,23,24

45 C INDEX I LOCATES EQUATION TO BE USED FOR ELIMINATING THE NTH

C VARIABLE FROM THE REMAINING EQUATIONS

50 C INTERCHANGE EQUATIONS I AND NN

C

28 IF(NN-1) 29,31,29  
29 DO 30 J=NN,IUSE1

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```

55      Z=G(I,J)
      G(I,J)=G(NN,J)
      G(NN,J)=Z
      30 CONTINUE
      C
      C-----DIVIDE-NTH ROW BY NTH DIAGONAL ELEMENT AND ELIMINATE THE NTH
      C VARIABLE FROM THE REMAINING EQUATIONS
      C
      31 K = NN + 1
      DO 36 J = K, IUSE1
      36 IF((I,NN).EQ.0.) GO TO 23
      -       G(NN,J) = G(NN,J) / G(NN,NN)
      36 CONTINUE
      IF(K-IUSE1) 86,45,46
      86 DC 44 I = K,IUSE
      40 GO 44 J = K,IUSE
      41 G(I,J) = G(I,J) - G(I,NN)*G(NN,J)
      44 CONTINUE
      45 CONTINUE
      C
      C BACKSOLVE FOR THE VARIABLES
      C
      75   K = IUSE
      47   J = K + 1
      C
      X(K) = 0.000
      X(JK) = 0.0
      SUM = 0.0
      104 48 IF(IUSE - J) 51,46,46
      46 DC 50 I = J,IUSE
      -       SUM = SUM + G(K,I)* X(I)
      50 CONTINUE
      51 X(K) = G(K,IUSE1) - SUM
      K = K - 1
      52 IF (K) 47,151,47
      23 IUSE = IUSE-1
      151 RETURN
      END
  
```

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